## PREFACE

This annual report reviews the research activities of the Laboratory of Advanced Science and Technology for Industry (LASTI) in the academic year of 2012 (April 2012 –March 2013) including activities using a 1.5GeV synchrotron radiation facility "NewSUBARU" and compact 15-MeV linac "LEENA" at the site of SPring-8. Other research activities of the micro and nanoscale carried out energetically at CAST building.

Topics of the NewSUBARU research activities of this year are as follows. First is achievements of a small linear electron accelerator LEENA. This accelerator was reconstructed and generation of THz Smith-Purcell radiation was started. Second is developments of LSI mask pattern observation system for extreme ultraviolet lithography (EUVL) using lensless scatterometry microscope. Third is a new irradiation hutch for gamma-ray beam source was added by collaboration with Konan University. The user use of gamma-ray beam of photon energy up to 76.3 MeV was started. Generating maximum gamma-ray power was 0.33mW. Fourth is the top-up beam current of NewSUBARU was enhanced from 250 mA to 300 mA. This was achieved by longer lifetime as a result of an additional installation and optimization of sextupole magnet families.

Furthermore, most of our research activities are being conducted in collaboration with industries, government research institutes and other universities. NewSUBARU beamlines are intensively used by companies. We will continue to respond to the community's demand by offering new science and technologies.



Shuji Miyamoto

Director of LASTI University of Hyogo

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#### The organization



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## **Current Status of NewSUBARU**

#### **Beamlines**

Takeo Watanabe and Hiroo Kinoshita Center for EUVL, LASTI, University of Hyogo

Total nine beamlines are operating in the NewSUBARU synchrotron facility. Four beamlines of BL01, BL03, BL06 and BL11 were constructed until 1999. Three beamlines of BL07, BL09 and BL10 were started the operation from 2000.

BL03B beamline branched from the BL03 beamline propose for the usage of the EUVL (extreme ultraviolet lithography) microscope for the EUVL finished mask inspection.

BL09B beamline branched from BL09 beamline for the usage of the usage of the EUV interference lithography to evaluate. And BL09C beamline branched from BL09B

beamline for the usage of the thickness measurement of the carbon contamination originated to the resist outgassing during the EUV exposure.

BL02 beamline was constructed for the usage of LIGA in 2003.

BL05 beamline was constructed in response to a demand in the industrial world in 2008, that is enhancement of the analysis ability in the soft X-ray region with the development of nanotechnology.

The arrangement of the beamlines in the NewSUBARU synchrotron radiation facility is shown in Fig.1.



Fig. 1 Beamline arrangement in NewSUBARU.

#### I. BL01

BL01 is a beamline for research and developing new

light sources. This beamline is one of two long

straight section on NewSUBARU. Optical klystron was installed at this straight section. Upstream side of this beamline (BL01B) is intended to be used for visible and infrared light generated from FEL or SR. Downstream side of this beamline (BL01A) is used for laser Compton scattering gamma-rays source. Gamma-ray beamline hutch just outside of the storage ring tunnel was constructed in 2004 for gamma-ray irradiation experiments. Specifications of this gamma-ray source are listed in Table 1.

Table 1.	Specification	of BL01	gamma beam
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	¥
CO <sub>2</sub> laser	Gamma energy : 1.7 - 4 MeV
10.52 μm	Gamma flux* : 9 x106 γ/s
5W	: 6 x105 γ/s (1.5-1.7 MeV)
	(with 3mm collimator)
Nd laser	Gamma energy : 17 - 40 MeV
1.064 μm	Gamma flux* : 7.5 x106 $\gamma$ /s
0.532 μm	: 3 x105 γ/s (15-17 MeV)
5 W	(with 3mm collimator)

\*Electron beam energy : 1-1.5 GeV \*Electron beam current : 250 mA

gamma-ray beam divergence : 0.5 mrad

#### II. BL02

The LIGA (abbreviated name of Lithogaphic, Galvanoformung and Abformung) process which consists from deep x-ray lithography, electroforming, and molding process is one of the promising candidates for such 3D micofabrication. More than hundreds aspect ratio for microstructure can be attained by the usa of the higher energy x-rays (4-15 keV) from synchrotron radiation (SR) with deeper penetration depth to the photosensitive resist. In this system we have succeeded to enlarged the exposure area up to A4 size and the fabrication dimension from submicron to millimeter by varying the energy of the x-ray source in accordance with the size of desired microparts. Micostructure with high aspect ratio over several hundreds will bi achieved using the x-rays over 10 keV since high energy x-ray has deep penetration depth to the photo-sensitive resist materials. Whereas, in the case of lithography for low energy x-rays from 1 keV to 2 keV, submicron structures with high aspect ratio will be achieved using the x-rays mask with precise line-width and thinner absorber, since low energy x-rays has low penetration depth. Based on this principle, the beamilne for x-ray exposure have constructed with continuous selectivity of x-rays frpm 100 eV to 15 keV by using the New gamma-ray irradiation hutch "GACKO" was installed at BL01A, collaborating with Konan University. Table 2 shows the specification of "GACKO".

Table 2	. Spe	cification	of "C	JACKO'
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1	
Maximum gamma-ray power	0.33 mW
Maximum gamma-ray energy	1.7MeV - 73 MeV
CO2 laser, wavelength/power	10.59µm/10W
1-1.7MeV gamma-ray flux	2×10 <sup>^7</sup>
	γ/sec@10W/300mA
Nd:YVO4 laser, wavelength/power	1.064µm/ 30W,
	0.532µm/20W
10-17 MeV gamma-ray flux	5×10 <sup>^7</sup>
	γ/sec@30W/300mA

x-ray mirrors (plane and cylindrical mirror) and Be film filters. The horizontal angle of the outgoing SR could be obtained up to 12.5 mrad, which corresponds to the horizontal size of 220 mm (A4 horizontal size) at the exposure position. The second characteristic performance of the beamline is the high efficiency differential pumping system. This was necessary for maintain the vacuum difference between the storage ring (<10<sup>-9</sup> Pa) and the end-station (<10<sup>-9</sup> Pa) at which gasses for substrate cooling will be introduced in the exposure apparatus.

The flexibility for the shapes and functions of microstructure will be enlarged by achieving 3D microfabrication process using multi step exposure at various configuration between x-ray mask and substrates. The relative positions between x-ray mask and substrates, tilt and rotation angle to the SR incident direction can be moved simultaneously during SR exposure using 5 axis stages. The movement of each axis is controlled by the PC in terms of the scanning speeds, scanning length, and repetition number. In order to decrease the heat load of sample substrate suffered during SR irradiation helium introduction and substrate cooling mechanism were alse equipped. Specification of spectrometer is listed in Table 3.

Optics	Plane and cylindrical mirror, Be filters
Exposure energy	100 - 2 keV, and 4 – 15 keV
Exposure method	Proximity and multi step exposure
Wafer size	A4 or 8 inch
Exposure area	230 mm(H) ×300 mm(V)
Exposure environment	< 1 atm (He-gas)

Table 3. Specification of the LIGA exposure system

#### III. BL03

BL03 is a beamline for the developing the next generation lithographic technology so called extreme ultraviolet lithography (EUVL). The exposure tool is installed at the end station. Using this exposure tool, the research and development of the next generation lithography such as the less than 70 nm node is going on process. The exposure wavelength is 13.5 nm.

The semiconductor industry plays a very important role in the information technology (IT). In 2006, 256 Gbit DRAM with a gate length of 70 nm will be demanded in the IT industry. The extreme ultraviolet lithography (EUVL) is a promise technology for fabricating a fine pattern less than 70 nm. To meet this schedule, this technology has to be developed in the pilot line until 2004. As for the practical use, it is very important that both to achieve large exposure area and to fabricate fine patterns. Therefore, at Himeji Institute of Technology, large exposure field EUV camera consists of three aspherical mirrors was developed. First in the world, we fabricated 60 nm line and space pattern in the large exposure area of 10 mm×10 mm on a wafer. Furthermore, BL03B beamline branches from the BL03 beamline propose for the usage of the EUVL microscope for the EUVL finished mask inspection. Table 4 shows the specification of ETS-1.

 Table 4. Spectification of the exposure tool (ETS-1)

Imaging opticsThree aspherical mirrorsExposure wavelength13.5 nmNumerical aperture0.1Demagnification1/5Resolution60 nm	
Exposure wavelength13.5 nmNumerical aperture0.1Demagnification1/5Resolution60 nm	
Numerical aperture0.1Demagnification1/5Resolution60 nm	
Demagnification 1/5 Resolution 60 nm	
Resolution 60 nm	
Depth of focus 0.9 µm	
Exposure area (static) 30 mm×1 mm	
Exposure area (scanning) 30 mm×28 mm	
Mask size 4 inch, 8 inch, and ULE 6025	
Wafer size 8 inch	
Exposure environment In vacuum	

#### IV. BL05

BL05 was constructed in response to a demand in the industrial world, that is enhancement of the analysis ability in the soft x-ray region with the development of nanotechnology. BL05 consists of two branch lines for use in the wide range from 50 eV to 4000 eV. BL05A and BL05B are designed to cover the energy range of 1300-4000 eV and 50-1300 eV, respectively. The incident beam from the bending magnet is provided for two branch lines through different windows of a mask. Therefore, these two branch lines can be employed simultaneously.

1) The double crystal monochromator was installed at the BL05A. InSb crystals and Si crystals are prepared for a double-crystal monochromator. Toroidal mirrors are used as a pre-mirror and a focusing mirror of BL05A. XAFS measurement in the total electron yield mode and fluorescence XAFS measurement using SSD (SII Vortex) can be performed. The fluorescence XAFS spectra can be measured for samples at the end station filled with He gas. Table 5 shows the specification of monochromater.

 Table 5. Monochromator specification

Monochromator	Double crystal monochromator
Monochromator crystals	InSb(111), Si(111)
Energy range	1300-4000 eV
Resolution	E/_E=3000

2) The constant-deviation monochromator consisting of a demagnifying spherical mirror and a varied-line-spacing plane grating (VLSPG), which can provide high resolution, simple wavelength scanning with fixed slits, was mounted on BL05B. The optical system consists of a first mirror (M0), a second mirror (M1), an entrance slit (S1), a pre-mirror (M2), and three kinds of plane grating (G), an exit slit (S2) and a focusing mirror (M3). The including angle of the monochromator is 175°. Two measurement

chambers are prepared at the end station of BL05B. The XAFS spectra in the total electron yield mode and fluorescence XAFS spectra using SDD (EDAX) can be measured in a high vacuum chamber. In addition, the photoelectron spectrum can be measured using spherical electron analyzer (VG Sienta, R3000) in an ultra high-vacuum chamber. The chambers can be replaced by each other within 1 hour. Table 6 shows the specification of the monochromator.

 Table 6. Monochromator specification

Varied-line-spacing plane grating monochromator
100 l/mm, 300 l/mm, 800 mm/l
50-1300 eV
E/ZE=3000

#### V. BL06

BL06 has been mainly developed for irradiation experiments such as photochemical reaction, SR-CVD, photo-etching, surface modification. The white radiation beam from bending magnet is introduced to the sample stage using a pair of mirror, whose incident angle was  $3^{\circ}$ . The SR at BL06 sample stage had a continuous spectrum from IR to soft x-ray, which was lower than 1 keV. A

#### VI. BL07A and BL07B

This beamline was designed for the development of new materials by SR technology. This beamline consists of two branch lines, which are provided with an incident beam from a 3-m undulator by switching the first mirror. One of them is a high photon-flux beamline with a multilayered-mirror monochromator for the study of SR-process (BL07A) and another is a high-resolution beamline with a varied line spacing grating monochromator for the evaluation of nano-structure characteristics by SR-spectroscopy (BL07B). The useful range of emitted photons from 50 to 800 eV is covered at both beamlines. The light source of BL07 is a 3-m length planar undulator, which consists of 29 sets of permanent magnets, a period length of which is 76 mm. The incident beam from the undulator is provided for two branch lines by translational switching of first mirror.

differential pumping system can be utilized for experiments in a gas atmosphere, which is difficult in the soft x-ray region. A sample holder can install four pieces of samples at a time. By using heater set in the sample holder, the sample can be heated from room temperature to 220°C. The temperature of sample is monitored using a Cr-Al thermocouple mounted on the sample holder.

#### 1) BL07A

The multilayered-mirror (MLM) monochromator, which has high reflectivity in the soft X-ray region, was installed at the BL07A. It consists of a switching mirror chamber, a slit chamber, a MLM monochromator, a filter chamber and a reaction chamber. To obtain a large photon flux, we decided to use only first mirror (switching mirror), M0, for focusing. The MLM monochromator is designed to cover an energy range of up to about 800 eV by combination of three kinds of mirror pairs with 4 kinds of filter. The flux deliver by this design is estimated to be between a maximum of  $10^{17}$  photons/s at 95 eV and a minimum  $2 \times 10^{14}$  photons/s at 300 eV for a 500 mA ring current. Table 7 shows the summary of BL07A.

		14,		1 $j$ $0 $ $1$ $D $ $L $ $0 / 1 $ $1$			
Energy		M	ultilayer mirr	or		Fil	ter
range	Material	spacing	Thickness	number of	$\Delta E/E$	material	Thicknes
(eV)			Ratio	layers			s
50-60	/					Al	100 nm
60-95	Mo/Si	20 nm	0.8	20	6.2 %		
90-140						None	
140-194	Mo/B <sub>4</sub> C	11 nm	0.5	25	3.3 %		100
190-400						Ag	100 nm
400-560	Ni/C	5 nm	0.5	60	2.5 %	Cr	500 nm
550-800						Ni	500 nm

Table 7. Summary of BL07A

#### 2) BL07B

The constant-deviation monochromator consisting of a demagnifying spherical mirror and varied line spacing plane grating (VLSPG), which can provide to high resolution, simple wavelength scanning with fixed slits, was mounted on BL07B. The optical system consists of a first mirror (M0), a entrance slit (S1), a premirror (M1), and three kinds of plane grating (G), an exit slit (S2) and a focusing mirror (M2). The monochromator is designed to

cover the energy range 50-800 eV with three gratings, of which including angle are 168°. The VLSPG has been well known to obtain high resolution in extreme ultraviolet region by diminishing various kinds of aberration. The total resolving power about 3000 can be realized in the whole energy region. Table 8 shows the specification of the monochromator.

 Table 8. Monocromator specification

Mount type	Hettrick-Underwood type
Grating G1, G2, G3	Plane VLS (600 l/mm, 1200 l/mm, 2400 l/mm)
Energy range	50-150 eV, 150 – 300 eV, 300-800 eV
Resolving power $(E/\Delta E)$	~3000

#### VII. BL9

A purpose of this beamline is studies on a soft x-ray interferometry or a holographic exposure experiment with making use of highly brilliant and coherent photon beams radiated from 11 m long undulator in NewSUBARU.

BL09 consists of M0 mirror, M1 mirror, G grating and M2 and M3 mirror. M0 and M3 mirrors are used for horizontal deflection and beam convergence, M1 is used for vertical beam convergence at the exit slit, and M2 is used for vertical deflection and beam convergence. A monochromator is constructed by M1 and a plane grating. The maximum acceptance of the undulator beam is 0.64 mrad in horizontal and 0.27 mrad in vertical. The

acceptance can be restricted by 4-jaw slits equipped at upstream of the M0 mirror.

BL09B beamline branched from BL09 beamline for the usage of the EUV interference lithography for the evaluation of the exposure characteristics of EUV resist. Coherence length of 1 mm at the resist exposure position was achieved using BL09B beamline. And BL09C beamline branched from BL09B beamline for the usage of the thickness measurement of the carbon contamination originated to the resist outgassing during the EUV exposure. Table 9 shows the specification of the monochromator.

Table 9. Monochromator specification

	moemoniator speetheatton
Mount type	Hettrick-Underwood type
Grating	Plane VLS (900 l/mm)
Energy range	50 - 600  eV
Resolving power (E/ $\Delta$ E)	$\sim 3000$

#### VIII. BL10

BL10 is for the global use in the Himeji Institute of Technology. M0 mirror is used for horizontal deflection and beam convergence, M1 is used for vertical beam convergence at the exit slit, and M2 is used for vertical deflection and beam convergence. A monochromator is constructed by M1 and a plane grating. At the beginning, the multiplayers reflectiveity measurement was carried out at this beamline. The characteristics of this beamline and the result of the Mo/Si multiplayers measurement are carried out for the development of the EUVL mask technology.

BL10 utilizes a monochromator of the varied line spacing plane grating monochromator (VLS-PGM). The line density of the monochromator in central region of the grating is 600 lines/mm. The reflectometer is a two axis vacuum goniometer using two Huber goniometers. One axis carries the sample, which may for examplee be a mirror at the center of the reflectometer vacuum tank ( $\theta$ -motion). The other ( $\varphi$ -motion) carries the detector on a rotating arm. In addition there are through-cacuum linear motions to translate the sample in two orthogonal directions (x,y). All motors are controlled by computer. The sample itself is mounted on a kinematic holder. The controlstage monochromator rotation, and data analysis were program using LABVIEW software. The reflectivity result obtained at BL10 has a good agreement with that at LBNL.

The mirso-CSM tool was adapted at the most downstream of the BL10 beamline fot the EUV mask defect inspection. This too is very effective for the inspection of the actinic patterned mask. Table 10 shows the specification the monochromator.

 Table 10. Monochromator specification

Mount type	Hettrick-Underwood type
Grating	Plane VLS (600 l/mm)
Energy range	50 - 600  eV
Resolving power (E/ $\Delta$ E)	$\sim \! 1000$

#### IX. BL11

A beam line BL11 is constructed for exposure Hard X-ray Lithography (DXL) in the LIGA (German acronym for Lithographite Galvanoformung and Abformung) process. LIGA process, that utilizes a useful industrial application of SR, is one of the promising technologies for fabrication of extremely tall three-dimensional microstructures with a large aspect ratio. This process was invented at the Institut Fur Mikrostrukturtechnik (IMT) of Karlstuhe Nuclear Center (KfK) in 1980. the Microstructures with height of over a few hundreds µm have been widely applied to various fields such as micro-mechanics, micro-optics, sensor and actuator technology, chemical, medical and biological engineering, and so on. This beam line was designed by the criteria ; photon energy range 4 keV to 6 keV, a beam spot size on the exposure stage  $\geq 50 \times 5 \text{ mm}^2$ , a density of total irradiated photons  $\geq 10^{11}$  photons/cm<sup>2</sup>. BL11 of an absorber chamber, a first-mirror chamber (M1), a second-mirror chamber (M2), a 4-way slit chamber, a Be window chamber, and an exposure chamber. The second pre-mirror is bent elliptically using a bending mechanism.

Fine bending adjustment of the M2 mirror can be made in the UHV by the pulse motor. The LIGA process needs the photon energies of 3 keV to 6 keV, the optics of a LIGA beam line generally employ a Pt monolayered-mirror and a Be window, which cuts off low-energy photons. The reflectivity of a Pt-coated mirror is about 55 % in the range of photon energy from 2 keV to 4 keV, however, it drops to 30 % at the photon energy of 6 keV. Therefore, new materials with a high reflectivity must to be found for Deep X-ray lithography (DXL) in this energy range. We propose the use of a Ni/W/C multilayered-mirror with a graded d-spacing in the range of photon energy from 3 eV to 6 keV. The calculated reflectivity of the Ni/W/C multilayered-mirror is higher than 56 % at the photon energy of 6 keV with a glazing incident angle of 0.8 degrees, and photons that have higher photon energy than 6 keV can be removed A 200 µm-thick beryllium (Be) window in a Be window chamber is used to separate the ultra-high vacuum part from the low vacuum part and to cut off low-energy photons. Table 11 shows the specification of the LIGA exposure system.

iubie iii speeineunen er m	e Eron enposare system
Exposure method	Proximity exposure
Wafer size	4 inch
Exposure area	50 mm(H)×80 mm(V)
Exposure environment	< 1atm (He-gas)
Exposure environment	< 1atm (He-gas)

 Table 11. Specification of the LIGA exposure system

### NewSUBARU Storage Ring

Y. Shoji

#### **Storage Ring Parameters**

The machine parameters of the 1.5 GeV storage ring are listed in Table I. Although the machine condition remains the same, some of the values are revised according to the new model calculation.

Table I	Main parameters of the NewSUBARU
storage 1	ing in FY2011.

Circumference	118.73 m				
Bending lattice type	modified DBA				
Number of bending cells	6				
Straight sections	4m X 4, 15m X 2				
Bending radius	3.22 m				
Injection energy	1.0 GeV				
Maximum energy	1.5 GeV				
RF frequency	499.955 MHz				
Betatron tune	6.29 (H), 2.23 (V)				
Momentum compaction fa	ctor 0.0014				
Electron energy	1.0 GeV 1.5 GeV				
RF voltage	100 kV 260 kV				
Natural energy spread	0.047% 0.072 %				
Natural emittance	50 nm 112 nm				
Maximum beam current	500 mA				

#### **Operation Status**

The ring has two user-time operation modes, 1.0 GeV top-up operation mode and 1.5 GeV operation mode. The basic operation time is 9:00 - 21:00 of weekdays. Monday is used for machine R&D, Tuesday is for 1.5 GeV user time, Wednesday and Thursday are for 1.0 GeV top-up user time, Friday is for 1.0 GeV or 1.5 GeV user time. Night period or weekend is used for machine study and user time with the special mode, single bunch operation and Laser-Compton Gamma ray, if necessary.



Figure 1: Machine time in FY2012.

The total machine time in FY2011 was 2661 hrs, 115% of that of FY2011, including the beam down time. Fig. 1 shows the breakdown. The beam down time includes not only the down by a failure, but also off-beam periods by a beam abort or others due to the beam instability. The category 'beam line commissioning' had been included in the user time until FY2011. The total of the normal user time and the beam line commissioning in this FY, 1850 hrs, was about 121% of that in FY2011. Time for machine study and special users was 128% of that in FY2011. The down time due to the machine trouble was 1.0%, the same level with that in FY 2011.

#### **Machine Troubles**

The machine troubles in FY2012 are listed in Table II. The rate of hardware troubles was increasing. We had troubles in two different timing modules. The synthesizer, which is used as a 500MHz master signal generator, had a trouble in AC-DC units and the signal became noisy. This was not counted in down time because we could continue user operation. We had troubles in 5 magnet power supplies.

#### **Machine Study and Special User Time**

Table III shows the list of machine studies in FY 2012. One special theme, a research related to a production of Laser-Compton backscattering  $\gamma$ -ray and its use, took more than 50% of the machine study time. Most of them took place after the completion of the new  $\gamma$ -ray hatch at BL1 in November 2012.

Most of the study reports are open to the public on the home page of NewSUBARU ( http://www. lasti. u-hyogo. ac. jp/ beam\_physics/ NewSUBARU).

#### **Accelerator Improvements**

The top-up operation current has been raised from 250 mA to 300 mA since October 2012. Fig.2 shows typical operation in these 5 years. This improvement was achieved by longer lifetime as a result of an additional installation and optimization of sextupole magnet families. The harmonic sextupole family named 'S1' was separated to 'S1', 'S3OK', and 'S3LU' and they were connected to the independent power supplies.

New vertical kicker magnet system was installed at one of the long straight sections. Its pulse shape was 450 ns width half sine, a little bit longer than the revolution period. The main purpose of the installation was the accelerator physics research to generate narrow band coherent THz radiation. However it is useful also for various researches and machine parameter measurements.



Figure 2: Improvement of top-up operation current in these 5 years.



Figure 3: Newly installed vertical kicker system.

Group	Failure/trouble	beam down time (hr)
Operation	Miss operation (human error)	0.9
Operation	Beam loss by a beam instabilities	3.6
	Schedule delay by SPring-8 trouble	2.3
RF & Timing	Timing module	11.3
	Synthesizer (noisy signal)	0.0
Magnet	Power supply	3.7
Beam monitor li	ne Cooling water leak at SR5	5.2
Utility	Electric power down by a thunder	0.4

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Table II Machine troubles in FY2012.

Table III List of machine studies in FY2012. The unit of study time is counted by shifts (typically 12 hrs).

R&D theme and special user mode	responsible person	study shift
Laser-Compton backscattering $\gamma$ -rays	S. Miyamoto	33
Parameter tuning for various energy operations	S. Miyamoto	1
Commissioning of visible light profile monitor port SR5	Y. Shoji	5
Skew quadrupole coupling correction	Y. Shoji	6
Coherent synchrotron oscillation feed-back	Y. Shoji	1
Betatron amplitude dependent orbit shift	Y. Shoji	1
Coherent synchrotron radiation by chromaticity modulation	Y. Shoji	9
Linear lattice model confirmation	Y. Shoji	1
Commissioning of the multi-element corrector	Y. Shoji	6
Identification of RF noise source (synthesizer trouble)	Y. Shoji	2

# **Research Activities**

## Tentative Design Parameters of 1.5 GeV Injector Synchrotron for New SUBARU

#### Y. Miyahara New SUBARU, LASTI

#### Abatract

So far, an electron beam has been injected in the New SUBARU storage ring from the SPring-8 injector linac at 1.0 GeV, but this system is not necessarily permanent. To prepare for an unexpected situation, 1.5 GeV injector synchrotron for the storage ring was considered. Design parameters of the synchrotron and the beam transport from the synchrotron to the storage ring are presented. An improved performance is expected by the top-up injection at the higher energy.

#### 1. Comparison of injection parameters

Injector		SP-8 linac	NS synch	NS-linac
Injection energy	E <sub>in</sub> (GeV)	1.0	1.5	0.05
Energy spread	$\delta E/E_{in}(\%)$	1.0	0.06	1.0
Emittance	$\varepsilon_{xin}$ (rad m )	$100*10^{-9}$	$208*10^{-9}$	$1*10^{-6}$
Inj. beam size	$\sigma_x(mm)$	1.0	1.4	5
Pulse Current	$\Delta I(mA)$	0.5	0.5	2.5
Charge	$\Delta Q(nC)$	0.2	0.2	1.0
Initial inj. period.	$\tau_{in}(s)$	1.0	1.0	1.0
Top up inj period	$\tau_{tp}(s)$	30	30	30
Stored current	$I_0(mA)$	250	250	
Inj. time	$\Delta t(min)$	10	10	10

#### 2. NS Synchrotron

1)	Lattice					
	Beam energy		$E_0 E_{inj}$	GeV)	1.5, 0.05	
	Circumference		C (m)		59.364	
	Symmetry		Ns		4	
	Average radius		R (m)		9.4483	
	Momentum con	mp. fac.	$\alpha_{\rm p}$		0.0683	
	Energy spread		$\sigma_{\rm E}/{\rm E_0}$		6.0x10	
	Tune		$Q_x, Q_y$		3.25, 2.15	
	Natural chroma	aticity	$\xi_x, \xi_y$		3.35, 4.14	
	Emittance	2	$\varepsilon_x(nmra)$	d)	208	
	Twiss param	$\beta_{xmax}, \beta_{vmax}$	$n_x, \eta_{xmax}$ (	(m)	8.03, 15.39, 2.08	
	Bend mag (rec	t angular)	in the second seco		, ,	
	U V	Field	B (T)		1.1, (0.0366)	
		Length	$l_{\rm B}(m)$		2.3815	
		Number	N <sub>B</sub>		12	
	Quad mag			~		
	Field	strength	$K_{F_{i}} K_{F_{i}}$	<sub>D</sub> , (m)	2.5243, -2.3465	
	Leng	th	$l_F, l_D$		0.35, 0.3	
	Num	ber	$N_Q$		12x2	
	Operation					
	Repetition	$f_R(Hz)$		1		
	Single bunch					
	Extraction					
	1		Le	ength(m)	Field(T)	Angle(deg)
	Kicker	K <sub>ex</sub>		0.4	0.02	0.26
	Bump	Bu		0.2	0.04	0.26
	Septum	SP3(pul	se) (	).3	0.4	1.37
		SP4(D	C)	1.2	1.2	15.1

	On-axis Injection Septum Kicker	SP <sub>in</sub> K <sub>in</sub>	0.4 0.2	
2)	<b>RF system</b> Revolution freq. RF freq Harmonic num. RF voltage RF bucket height Synchrotran tune Bunch length	$\begin{array}{c} f_0 \ (MHz) \\ f_{RF} \ (MH) \\ h \\ V_{RF} \ (MV) \\ \Delta E_{RF}/E_0 \\ Qs \\ \sigma_\tau \ (ps) \end{array}$	) z) /)	5.05 500 99 4 (0.2) 0.016 (0.019) 0.054 0.24
3)	Vacuum Pressure (in beam) Below chamber Pump station	P (Torr) H*V (m N <sub>P</sub>	um²)	10 108x34 12
4)	Monitor Position Beam current Tune monitor	N <sub>pm</sub> fast, slov	v	12 1 + 1
3.	Injector linac			
Bea RF Ene Rep Puls Puls Emi	m energy freq rgy spread se length se electron ittance	$\begin{array}{c} E_{inj} \left( MeV \\ f_{RF} \left( MHz \\ \delta E/E \right. \left( \% \right) \\ f_r \left( Hz \right) \\ l_p \left( ns \right) \\ n_e \\ \epsilon_x (rad \ m) \end{array}$	(i) $+/-$	$50 \\ 2856 \\ 1.0 \\ 1 \\ 1 \\ 10^{10} \\ 10^{6} $
<b>4.</b>	Beam Transport			
INCV	Bend N <sub>B</sub> B	(T)	3	
	$\begin{array}{c} & & & l_{\rm B} \\ {\rm Quad} & & {\rm N} \\ & & & l_{\rm Q} \end{array}$	(m) Q (m)	1.349, 2 11 0.25, 0.3,	.382 0.35
Old	(necessary to check	k PS and Mag	g)	
	Bend M	N <sub>В</sub> В (Т)	1 (necessa 0.933 (assu	ry to reconstruct) umed,)
	Quad $N_{l_Q}$	<sub>3</sub> (m) Q (m)	1.215 (assu 10 0.25, 0.3, 0	med) .35
Bea Stee Vac	m position monitor ering mag uum pump			



Fig.1. Layout of 1.5 GeV injector synchrotron

Fig.2. Lattice functions of synchrotron



Fig.3. Beam transport from synchrotron to storage ring





(a) First straight section around B0 to B1

(b) 2nd straight section around B1 to B2



(c)  $3^{rd}$  straight section around B2 to B3



## Calibration of Pyrgeometer by Blackbody Radiation with RMS method on New Steady State Equation of Heat Transfer

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#### Abstract

Calibration of pyrgeometer was performed using blackbody radiation, for which a new steady state equation of heat transfer in the pyrgeometer was developed. Expansion coefficients in the equation were determined by rms method on the experimental data, which, however, depend much on the undefined constant  $\alpha$  of thermopile voltage used for temperature measurement in the pyrgeometer. The coefficients were also determined using numerical values of physical properties of its components. It was demonstrated for the first time that both coefficients well agree at a special value of  $\alpha$ .

#### 1. Introduction

Pyrgeometers, PIR of Eppley Laboratory Inc. and MS-200 of EKO Instruments for example, are widely used to measure infrared radiations, which coming down from the atmosphere around the earth. It is composed of silicon dome, sensor plate and The dome coated container (body). with anti-reflection layer, passes infrared but not visible wave. The sensor is connected to the body with heat conductor. Its calibration is performed by injecting a slowly varying blackbody radiation from a conical cavity, when temperatures of the cavity, dome and body  $(T_{\rm B}, T_{\rm d}, T_{\rm b})$  are precisely measured. A thermopile is used to measure voltage V due to temperature difference between sensor and body.

Calibration of PIR was originally performed on a steady state equation of heat transfer in considering dome effect [1], after which several investigations were reported. Typical example is as follows [2.3].

Measured data of  $X = \sigma(T_s^4 - T_d^4)$  and  $Y = \sigma(T_B^4 - T_s^4)$  are plotted on (X, Y) plane, and fitted with a straight line. Then, coefficients *a* and *k* in the following equation are determined as a = 246.3 W/m<sup>2</sup>/mV and k = 3.16 with errors of  $\Delta a = 10.3$  and  $\Delta k = 0.03$ ,

$$\sigma(T_B^4 - T_s^4) / V = a + k\sigma(T_s^4 - T_d^4) / V$$
(1)

where  $\sigma$  is the Stefan-Boltzmann constant and suffixes *B*, *s* and *d* stand for the cavity, sensor and dome, respectively. Practically, *T*<sub>b</sub> is used in place of *T*<sub>s</sub> since *T*<sub>b</sub> is very close to *T*<sub>s</sub>. The coefficients *a* and *k* are expressed as  $a = a'(1 - \rho_d \rho_s)/(\tau_d \varepsilon_s)$  and  $k = \varepsilon_d / \tau_d$ , where *a*' is transfer coefficient of thermopile,  $\rho$  the reflectance,  $\tau$  the transmittance, and  $\varepsilon$  the absorption coefficient.

Efforts have been made to improve the accuracy using more detailed equations [4~6]. In all cases, however, physically-expected values of *a*, *k* and others in the equations are not given explicitly. If we apply probable values  $\varepsilon_d = 0.05$  and  $\tau_d = 0.7$  in Eq.(1), for instance, we obtain k = 0.071, which is



**FIG. 1.** Schematic diagram of heat transfer in pyrgeometer. Multiple reflections of radiation between sensor and body are not drawn. Symbols are explained in text.

much different from the experimental value. For a long time, however, little attention has been paid to the disagreement, which can be solved by improving the steady state equation, as discussed below.

Above investigations are all based on the same assumption of heat transfer of radiations above the sensor and the one through the conductor. In the present study, we additionally consider three factors; 1) heat transfer between the sensor and body by radiations, 2) heat transfer from sensor to the air or gas in the body by convection, 3) form factor  $\Gamma_d = 2.094$  of semi-spherical dome for radiation convergence on the sensor (see **Fig.1**). Note that multiple reflections between sensor and body are not drawn in the figure to avoid complexity, and no multiple reflections between sensor and dome are

considered because of black surface of sensor upside.

Then, the steady state equation can be expressed as

$$\tau_{d}Q_{B} + \varepsilon_{d}\Gamma_{d}Q_{d} + \varepsilon_{s}\rho_{d}Q_{s} + F_{b}Q_{b} + F_{s2}Q_{s}$$
$$= (Q_{s} + \frac{Q_{h}}{\varepsilon_{s}}) + \frac{1-R}{\varepsilon_{s}}(\varepsilon_{s2}Q_{s} + Q_{h}) + \frac{R}{\varepsilon_{s}}Q_{c}$$
(2)

where symbols  $F_{b}$  and  $F_{s2}$ , are given by

$$F_b \equiv \frac{\varepsilon_{s2}}{\varepsilon_s} \varepsilon_b (1 + \rho_b \rho_{s2} + \rho_b^2 \rho_{s2}^2) (1 - R)$$
$$F_{s2} \equiv \frac{\varepsilon_{s2}}{\varepsilon} \varepsilon_{s2} \rho_b (1 + \rho_b \rho_{s2} + \rho_b^2 \rho_{s2}^2) (1 - R)$$

The left and right hand sides of Eq.(2) are the entering and go-out of heat with respect to the sensor, respectively.  $Q_x$  (x= B, s, b, d) =  $\sigma T_x^4$  is the radiation energy, and  $Q_c = (\lambda/L)(V/\alpha)$  is the heat transfer though the conductor with  $\lambda$  the heat conductivity and L the length, The heat transfer to the gas is given by  $Q_h = H_g (T_s - T_g)$ , where  $H_g$  is the heat transfer coefficient of  $H_g \approx 5 \text{ W/m}^2/\text{K}$  in no-stream gas. Suffix s<sub>2</sub> indicates the downside of the sensor. The voltage of thermopile is given by  $V = \alpha (T_s - T_b)$  with  $\alpha$  proportional constant. A<sub>s</sub> and A<sub>c</sub> are the area of

sensor and that of the cross section of conductor with  $R = A_c/A_s$ .

Eq.(2) can be simplified as

$$\delta Q \equiv Q_B + aV + sQ_s + bQ_b + dQ_d + hQ_h = 0$$
<sup>(3)</sup>

where a, s, b, d and h are expansion coefficients. Comparing Eqs.(2) and (3), we obtain

$$a^{*} = -\frac{1}{\alpha} \frac{R}{\varepsilon_{s}\tau_{d}} \frac{\lambda}{L}$$
(4a)  
$$= -\frac{1}{\tau_{s}} [1 + \frac{\varepsilon_{s2}}{\varepsilon} (1 - R)] + \frac{\varepsilon_{s}\rho_{d}}{\tau_{s}} + \frac{F_{s2}}{\tau_{s}}$$
(4b)

$$b^* = \frac{F_b}{\tau_d} \qquad d^* = \frac{\varepsilon_d}{\tau_d} \Gamma_d \qquad h^* = -\frac{(2-R)}{\varepsilon_s \tau_d} \tag{4b}$$

The coefficients are marked with (\*) to represent them as physically-expected values. Note that  $b^*$  and  $d^*$  are both positive, which becomes important later.

Experimentally,  $T_{\rm B}$ ,  $T_{\rm b}$ ,  $T_{\rm d}$  and V are measured at  $t_{\rm j}$  with j = 1~960, from which we can obtain optimum values of the expansion coefficients by applying rms method to Eq.(3). The coefficients are given by the solution of the following equation;

$$\begin{bmatrix}
\sum V_{j}^{2} & \sum V_{j}Q_{sj} & \sum V_{j}Q_{bj} & \sum V_{j}Q_{dj} & \sum V_{j}Q_{hj} \\
\sum Q_{sj}^{2} & \sum Q_{sj}Q_{bj} & \sum Q_{sj}Q_{dj} & \sum Q_{sj}Q_{hj} \\
\sum Q_{bj}^{2} & \sum Q_{bj}Q_{dj} & \sum Q_{bj}Q_{hj} \\
m_{ij} = m_{ji} & \sum Q_{dj}^{2} & \sum Q_{dj}Q_{hj} \\
\end{bmatrix}
\begin{bmatrix}
a \\
s \\
b \\
d \\
h
\end{bmatrix} =
\begin{bmatrix}
-\sum V_{j}Q_{Bj} \\
-\sum Q_{sj}Q_{Bj} \\
-\sum Q_{dj}Q_{Bj} \\
-\sum Q_{dj}Q_{Bj} \\
-\sum Q_{hj}Q_{Bj}
\end{bmatrix}$$
(5)

S

where the matrix is symmetric with  $m_{ij} = m_{ji}$ . The expected and optimum values ultimately should agree with each other. However, the agreement is reduced as the decrease of the completeness of steady state equation and experimental data.

#### 2.Experiment and analysis

Experiments were performed with MS-200 in the same way as [2.3]. It is placed upside down, and the dome is covered with the cavity. Alcohol and dry-ice are mixed to provide a low temperature liquid, which is circulated through a double-wall bath in the cavity. The liquid temperature, controlled by electric heater, is measured at several points to provide their average temperature  $T_{\rm B}$ . Nitrogen gas is softly brew upon the dome to change its temperature somewhat independently. The temperatures of inner surface of dome and body are measured with platinum resistances. The infrared radiation at the earth surface is about 270 W.m<sup>2</sup>, which corresponds to about -11 °C. At the same time, the voltage  $V = \alpha \Delta T$  is measured with a thermopile, which is composed of a series of 70~100 copper-constantan thermo-couples with a temperature coefficient of 0.043 mV/K each. Thus, the proportional constant is  $\alpha = 3.0$ ~4.3 mV/K. Time variation of measured temperatures is shown in **Fig. 2**.

In performing numerical calculation with Eq.(5), we take into account three undefined factors. The constant  $\alpha$  of  $V = \alpha \Delta T$  is not yet determined, and there is alternative possibilities of  $\Delta T = T_s - T_b$  and  $\Delta T = T_b - T_s$  since the connection is not quite sure. In addition, the gas temperature  $T_g$  is not measured. Accordingly, first we assume  $T_g = (T_s + T_b + T_d)/3$ , and scan  $\alpha$  for two possibilities of  $\Delta T$ .

CASE	a	s	b	d	h	<dq><sub>rms</sub></dq>	.α	$T_{g}(n)$
KA208	-238.09	-2.070	0.447	0.630	-7.957	0.367	3.4	$T_g(1)$
KA217	-240.30	-1.55õ	0.417	0.145	-10.48Ã	0.403	4.0	$T_{g}(1)$
KA218	-250.91	1.539-	0.421	0.124	-44.69õ	0.442	4.0	$T_{g}(2)$
KA219	236.0õ-	1.54 <b>8</b> -	0.420	0.135	-7.80Ĩ	0.341	4.0	$T_g(3)$
KA223	272.77 <del>-</del>	-2.90Ĩ	1.066	0.841	-17.05Ĩ	0.668	4.2	$T_g(1)$
KB 302	-213.23	-1.586	0.430	0.163	-3.106	0.419	3.96	$T_g(1)$
	a*	s*	b*	d*	h*			
Ex 22	-213 7Ã	-1 549	0 466	0 149	-2.85Õ			

Table 1  $\alpha$  dependence of expansion coefficients for V =  $\alpha(T_{b}-T_{s})$ 

Note :  $T_g(1) = (T_s + T_b + T_d)/3$ ,  $T_g(2) = (8T_s + T_b + T_d)/10$ ,  $T_g(3) = (2T_s + 4T_b + 4T_d)/10$ ,  $T_g(4) = (5T_s + 2.5T_b + 2.5T_d)/10$ 



**FIG. 2.** Time variation of measured temperatures,  $T_{\rm b}$ ,  $T_{\rm d}$ , and  $T_{\rm B}$  as well as thermopile voltage V.

First, we consider the case of  $V = \alpha(T_s - T_b)$ . The coefficients were calculated with Eq.(5) in the cases  $\alpha = 2.8 \sim 4.2$  at a step of 0.1. In all cases the rms errors are as small as  $\langle \delta Q \rangle_{\rm rms} = 0.3 \sim 0.8$  W/m<sup>2</sup>. However, these cases are all physically inadequate. As shown in Eqs.(4c),  $b^*$  and  $d^*$  are both positive, so that *b* and *d* are expected to be positive, but there are no such cases in the above calculations.

Second, we consider the opposite case of  $V = \alpha(T_b-T_s)$  The coefficients were calculated in the case of  $\alpha = 2.8 \sim 5.0$ . In these cases, the errors are also very small, and *b* and *d* are negative in almost all cases. However, we find both *b* and *d* are positive in the cases, KA208 ( $\alpha = 3.4$ ), KA209~211 ( $\alpha = 4.0$ ) and KA223 ( $\alpha = 4.2$ ), as shown in **Table 1.** 

Physically-expected values, which calculated with physical parameters given later, are shown by

Ex 22 in the bottom of the table. We see that total tendencies of the optimum and expected values well agree each other. Especially, all coefficients in the case of  $\alpha = 4.0$  agree very well, while *d* and *d*<sup>\*</sup> are considerably different in the cases of  $\alpha = 3.4$  and 4.2.

Among three cases KA217, 218 and 219 of  $\alpha$  = 4.0 in the table, we see that coefficient *h* varies substantially depending on  $T_g(n)$ , but other coefficients not so much. Thus, *h* dependence on ( $\alpha$ ,  $T_g(n)$ ) was surveyed as shown in **Fig.3**. The open and closed circles in the figure represent the cases where both *b* and *d* are positive and negative, respectively, and broken line represents the region of abs(h) < 6. Consequently, the most optimum values are obtained at  $\alpha = 3.96$  and  $T_g(1) = (T_s + T_b + T_d)/10$  with h = -3.1 compared with  $h^* = -2.8$ .

Finally, we discuss the physically-expected values. The silicon dome is coated for ant-reflection of infrared wave. Body and sensor are made of anodized aluminum. Upper surface of sensor is painted black. However, physical parameters (size and optical properties) of these components are not published. Then, we assume the following parameters;

 $\alpha = 3.96, \Gamma_{d} = 2.094, \lambda = 273 \text{ W/m/K}, L = 0.002 \text{ m}, R = 0.005, \varepsilon_{s} = 1.0 \\ \tau_{d} = 0.7, \rho_{d} = 0.25, \varepsilon_{d} = 0.05 \\ \varepsilon_{b} = \varepsilon_{s2} = \rho_{b} = \rho_{s2} = 0.5$ 

The expected values, which calculated with these parameters, are given by Ex 22 in **Table 1**. The transmittance of silicon crystal in infrared region, generally about 0.5, increases with the aid of anti-reflection coating, to about  $\tau_d = 0.7$ . It is known that absorption in the region is very small, so that  $\varepsilon_d = 0.05$  is assumed. Anodized aluminum, covered with porous oxide with a thickness of 10~200 µm, becomes glossy by machining, which approximately provides  $\varepsilon = \rho = 0.5$ . Parameter *R* is determined so as to make *a*\* close to *a*, since *a*\* depends much on *R*. Because *R* << 1, then *h*\* is automatically close to *h* 

 _ Term	B	a	s=====================================	====== b	 d	-==== h	 δQ	
$T_{\rm x}({\rm K})$	274.23	296.74	296.59	295.61	296.31			
$Q_{\rm x}({\rm W/m^2})$	320.68	-0.580	439.63	438.77	433.00	2.15		
x	1.000	-213.23̃	-1.586	0.430	0.163	-3.106		
$xQ_{\rm x}$ (W/m <sup>2</sup> )	320.68	123.67	-697.25	188.67	B70.58	-6.58	-0.23	
Note) $T_{\rm h}$	$=T_{g}=(T_{s}+T_{h})$	$+ T_{\rm d}$ )/3; $O_{\rm h}$ =	$=5(T_s-T_g)$	; $O_{a} = V(n)$	nV)			

**Table 2** Comparison of each term  $xQ_x$  in KB 302 ( $\alpha = 3.96$ ) at  $t_j = 500$ .

(= -3.1). The small value of *R* is probable if we imagine narrow bridges between the sensor and body. The form factor  $\Gamma_d = 2.094$ , numerically calculated in reference to **Fig.4**, makes the agreement better. If we set  $\Gamma_d = 1.0$ , we have  $d^* = 0.075$ , being much different from d = 0.163. For comparison, we apply the rms method to Eq.(1) with  $T_b$  in place of  $T_s$  on the present data, then we have a = 255.10 and k = 5.164 (while 0.071 expected) with  $\langle \delta Q \rangle_{\rm rms} = 1.46$ .

**Table 2** compares the magnitude of all terms at  $t_j = 500$  in the case of KB302 ( $\alpha = 3.96$ ). We see that the contribution of  $sQ_s$  in the total (=  $\delta Q$ ) is especially large, which is because radiation is emitted from both sides of sensor. The contribution of  $hQ_h$  is small, but not negligible compared with the error  $\delta Q$ . The temperature difference of  $T_s - T_b = 0.15$  K and  $T_s - T_g = 0.43$  K are small, but neither negligible to determine the optimum values.



**FIG. 3**, Optimum values of expansion coefficient *h* on  $(\alpha, T_g(n))$  plane.

In conclusion, a new steady state equation on heat transfer in pyrgeometer was developed by introducing three factors; 1) heat transfers between sensor and body, 2) heat transfer from sensor to the gas in body, 3) form factor for the convergence of dome radiation. Expected values of expansion coefficients of the equation were calculated using physical parameters of the components. Optimum values of the coefficients were also determined by rms method on the experimental data. It was found that expected and optimum values agree very well at a special value of  $\alpha$  with a very small error  $\langle \delta Q \rangle_{rms}$ . Further details and applications are discussed on the basis of the new steady state equation.



**FIG.4** Form factor  $\Gamma_{\rm d} = Q_{\rm 0sn}/Q_0$ , the ratio of radiations on the sensor and dome, is calculated in reference to this figure. Details are given elsewhere.

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## Preliminary Measurement of Solar and Atmosphere Radiations with a New Experimental Set-up of Double Copper Plate Structure

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#### Abstract

Solar and atmosphere radiations were measured with a new experimental set-up of double copper plate structure on fine calm days. In contrast to the conventional apparatus for all sky (global) radiation, there is no glass window in the set-up. The radiation analysis of measured data was performed in a simple clear algorism based on heat transfer by radiations. In spite of crude experiment, the results fairly well agree with the conventional ones, and are explained consistently using the Rayleigh scattering of solar radiation by air molecules with an atmosphere muddiness (turbidity) factor  $R_{\text{mud}} = 9.5$ , and similarly in regard to scattered radiation. However, it is not thought that the measured data are very accurate, so that it is required to improve the set-up and measurement for more detailed comparison. There is a large room to be improved.

#### 1. Introduction

In recent years, the warming climate on the earth is becoming a serious problem worldwide, so that the reduction of CO<sub>2</sub> and CH<sub>4</sub> gases in the atmosphere has become an urgent task in all countries. In fact, we experienced abnormal hot summer at a temperature as high as 35 °C for about two weeks two years ago. In the New SUBARU facility for a synchrotron radiation experiment equipped with an electron storage ring, the temperature in the experimental hall is controlled in the range of 25~26 °C by air conditioners. However, the electric power required for this is close to a contract limit. Accordingly, we have considered some measures for the air-conditioning to decrease the power. In order to see their effects beforehand, it is worthwhile to calculate the temperature distribution in the building before and after the measures.

Initially, we considered only the sunshine energy (solar radiation) on the roof. However, it was found that atmosphere radiation  $Q_a = \sigma_0 T_a^4$  (explained later) on the roof plays an important role to maintain the hall temperature at a moderate level whole day. If the radiation is not considered, the hall temperature decreases substantially at night. Accordingly, an appropriate expressions of the solar and atmosphere radiations are required. However, their introductory definitions and explanations found in Japanese internets are diverged in pieces, while discussions in articles and textbooks are rough or very advanced and detailed [1]. To get an approximate but physically consistent description as a whole, we have made a radiation analysis based on temperature measurements, which were obtained by an experimental set-up of double copper plate structure. The structure was prepared because of the similarity to the sunshine-on-roof problem.

The solar energy constant,  $E_{s0} = 1373 \text{ W/m}^2$  outside the atmosphere, is reduced considerably by scattering and absorption when passing through the atmosphere, and the atmosphere at a thermal equilibrium emits and reflects an infra-red radiation.

There are several types of special apparatus for the measurement of these radiations; pyrheliometer with a narrow window for solar radiation, pyranometer and pyrgeometer (infrared radiation monitor) for all-sky (global) radiation. By suppressing the solar radiation with a disk mask, the pyranometer can measure the scattered radiation. Examples of the radiation energies measured by the conventional apparatus in Japan Meteorological Agency are given in **Table 1**.

The solar radiation spectrum spreads out mainly in the wavelength  $\lambda = 0.3 \sim 3 \mu m$ , and longer at a lower level, with the peak at 0.5  $\mu m$ , while the infrared radiation at 300 K spreads in the range  $\lambda =$  $3\sim60 \mu m$  with its peak at 10  $\mu m$ . The top of pyranometer is covered with a glass window (dome), which is transparent up to 90 % almost in the same range as the solar radiation, so that this apparatus, when masked, is expected to measure the scattered radiation only.

The analytical algorism of pyranometer is that the temperature difference between detector plate and bottom base, measured with a thermopile, is proportional to the input of scattered radiation and inversely to heat transfer coefficient between them.

Table 1. Radiation energies measured with conventional apparatus

			U				11			
site	date	Ø	$E_{s_{2}}$	$E_{s} \sin \Theta_{2}$	$E_{all_2}$	$E_{\rm sc}{}_2$	$E_{sc}^{*}{}_{2}$	$Q_{\mathrm{IR}}$	$ au_0$	
		deg	W/m	W/m	W/m	W/m	W/m	W/m		
Fukuoka	12/4	33	943	512	600	71	88	260	2.7	
Tsukuba	3/17	55	771	632	857	228	225	260	5.1	
Tsukuba	3/19	55	814	667	843	171	176	280	4.7	

 $\Theta$ ;solar altitude,  $E_s$ ; solar radiation,  $E_{all}$ ; all sky radiation,  $E_{sc}$ ; scattered radiation,  $E_{sc}^* = E_{all} E_s \sin \Theta$ , expected scattered radiation,  $Q_{IR}$ ; infrared radiation,  $\tau_0$ ; atmosphere muddiness factor determined from  $E_s/E_{s0}$  (see Appendix A). All data are at noon. Tsukuba and Fukuoka are about 500 km away in the East and West, respectively, from the New SUBARU site.

The coefficient is mainly determined by the heat conductivity of support metal between the plate and base. The plate temperature is also affected by the radiation from plate surroundings. Accordingly, the transfer coefficient is carefully prepared, but its details are not explicitly described [2,3]. There is a good agreement between the measured radiation and the model-calculated one in the case of the solar radiation. However, there are considerable differences in some cases of scattered radiations [4-7]. Accordingly, there arose a question that thermal radiation of the glass window itself possibly affects the detector of pyranometer [8], and several results measured with pyranometers of different makers were compared [9].

On the other hand, as described in detail in section 2, the present set-up has no glass window, while surrounded with a wind suppressor. The measurement was performed on fine calm days of April 5<sup>th</sup> and 29<sup>th</sup> with no cloud in a light-blue sky, and no wind but with weak wind breathing. Plate temperatures were measured with thermometers. The structure is different from that of conventional apparatus. There is no need to consider the window effects, and the analysis is performed with an original algorism on the basis of heat transfer by radiations. Related energies and heat transfer in and out of the plates are considered explicitly and analyzed as a function of the solar altitude.

#### 2. Experimental set-up

The set-up is shown in **Fig.1**, which is placed horizontally in a dry-grass garden. To avoid or reduce the effects of wind and sunshine reflection from surrounding buildings, the set-up is about 10 m away from an office house, 5 m high, in the East, and about 30 m away from an experimental building, about 15 m high, in the North. There is no obstacle in the South and West. The set-up is surrounded by corrugated cardboard boxes with 460 mm high, being closely connected to suppress wind effects. The boxes in the opposite side against the sunshine are covered with a dark-blue cloth to suppress sunshine



**Fig.1.** Experimental set-up of double copper plate structure for solar and atmosphere radiation measurements; (a) side view and (b) top view. The set-up was placed in a dry-grass garden, on wood plates and corrugated board, and surrounded with corrugated board boxes.

reflection on the copper plates.

The measurement was performed for  $12:30 \sim 16:40$ , when the set-up was whole rotated gradually clockwise in accordance to the sunshine direction. The solar altitude  $\Theta$  was determined by measuring the shadow length of a square block placed on a horizontal plane.

On the other hand, for the measurement of atmosphere radiation in the garden, the set-up was placed in a shaded area, being produced by a white board,  $50x60 \text{ m}^2$  wide, and attached against sunshine on a three-leg support about 2 m high. The board and support were moved against the sunshine direction. In this case the wind suppressor was not placed since the weather was fine and very calm.



**Fig.2.** Measurement of radiation coefficient of copper plates. Temperatures of plate A and B measured by radiation monitor  $T_{radA}$  and  $T_{radB}$ , and those measured by conventional thermometer  $T_A$  and  $T_B$  are shown against nominal radiation coefficient  $\varepsilon_n$ . True coefficients  $\varepsilon_A$  and  $\varepsilon_B$  are determined at the point where both temperatures agree.



**Fig.3.** Radiations coming in and out of plates A and B. Meaning of symbols are given in the text.

As for the set-up, copper plates were used because of high heat conductivity for fast homogeneous response to the gradual change of solar radiation during the experiment. We tried to paint the plates with black color for complete absorption of radiation, but not successful because of its smooth surface. Instead, the radiation coefficient of the plates was determined from the surface temperature, being measured in a room with a thermal radiation monitor as well as the conventional monitors attached to the surfaces. Both surfaces of plate A are of dark orange color, and those of plate B are of metallic-mirror orange color.

**Figure 2** shows the temperatures  $T_{radA}$  and  $T_{radB}$  measured with the radiation monitor against the nominal radiation coefficient  $\varepsilon_n$  as well as the temperature  $T_A$  and  $T_B$  of plates A and B measured with the conventional monitors. From the figure, the radiation coefficient is determined as  $\varepsilon_A$ = 0.95 for plate A and  $\varepsilon_B$  = 0.90 for plate B. These nearly the same coefficients were not expected beforehand since plate B represents metallic mirror surface, but not plate A.

#### 3. Results and analysis

Figure 3 shows the expected transfer of radiation energy in and out of the copper plate A per unit area, where the downward radiation is composed of three parts;  $E_s$  the solar radiation,  $E_{sc}$  the scattered radiation, and  $Q_{IR}$  the infrared radiation. In the present experimental set-up of wide plates with a narrow gap, it is assumed that the radiations between the plates are emitted effectively in normal to the plates.

At first, we consider the shaded area measurement made for  $t = 13:11 \sim 16:35$ , when a set of temperatures  $T_A$ ,  $T_B$  and  $T_a$  at  $t_j$  (j = 1~28) were obtained. These temperatures at each set are mutually related as follows. At the equilibrium state, we have the following equation,

$$E_{sc} + Q_{IR} = p_A Q_A + p_B Q_B + p_H Q_H \qquad (1)$$

with the following definitions,

$$p_{A} = [2 - \varepsilon_{A}(1 - \varepsilon_{B})] ,$$

$$p_{B} = -\varepsilon_{B}[1 + (1 - \varepsilon_{A})(1 - \varepsilon_{B})], \quad p_{H} = 2/\varepsilon_{A}$$

$$Q_{A} = \sigma_{0}T_{A}(K)^{4} , \quad Q_{B} = \sigma_{0}T_{B}(K)^{4} ,$$

$$Q_{H} = H_{a}(T_{A} - T_{a})$$

where  $\sigma_0$  is the Stephan-Boltzmann constant, and  $H_a$  is the heat transfer coefficient between plate A and the air around the plate. Symbol K indicates the temperature unit of Kelbin. Heat transfer between the plates via air by conduction and convection is neglected since the heat conductivity of air is very small, and the air, slightly warmed between the plates, is thought to stream out before affecting the opposite plate.

Now, let's introduce an equivalent atmosphere radiation  $Q_{a0}$  in the sky as follows,

$$Q_{a0} = yQ_a = E_{sc} + Q_{IR} \tag{2}$$

where  $Q_a = \sigma_0 T_a(K)^4$ , and y is a constant to be determined. When Eqs.(1) and (2) are combined, y can be expressed as a function of  $H_a$ . Empirically, it is known that  $H_a \approx 5 \text{ W/m}^2/\text{K}$  for no air stream and  $10\sim300 \text{ W/m}^2/\text{K}$  for air stream, so that we first assume  $H_a = 5$ , 10 and 15 W/m<sup>2</sup>/K. Substituting measured temperatures  $T_A$ ,  $T_B$  and  $T_a$  at each set, we obtain y = 1.040, 1.058 and 1.076, respectively. As discussed later, however,  $H_a = 7.0 \text{ W/m}^2/\text{K}$  is the most probable in relation to the solar constant  $E_{s0}$ , and then  $y = 1.048 \pm 0.006$  is determined

Next, we consider the radiation measurement under the sunshine. From the measured temperatures,  $Q_n$ 's are expressed as a function of  $X (=\sin \Theta)$  (see **Fig.4**). Some fluctuations of the data are observed in the range of  $\sin \Theta = 0.5 \sim 0.8$ , which are caused by weak wind breathing and partly by the stepwise rotation of the set up as the sun moves. The weather was quite calm beyond the above range.



**Fig.4.** Radiation energy  $Q_A$ ,  $Q_B$ ,  $Q_a$  and  $Q_H$  measured under the sunshine against  $X (= \sin \Theta)$ , which are fitted by  $Q_n = a_n X + b_n + c_n / X$ .

again assume the Now. we equivalent atmosphere radiation  $yQ_a$  as Eq.(2), so that we have

$$E_s \sin \Theta = \sum_{n=A,B,H,a} p_n Q_n \tag{3}$$

where the fourth term  $p_aQ_a$  with  $p_a = y/\varepsilon_A$  is added. The experimental data  $Q_n$ 's are fitted by the following equations (see Fig.4),

$$Q_n(X) = a_n X + b_n + \frac{c_n}{X} \tag{4}$$

where  $a_n$ ,  $b_n$  and  $c_n$  are obtained as

$Q_{\rm n}$	$a_{\rm n}$	$b_{\rm n}$	$c_{n}$
$Q_{\rm A}$	391.7	262.2	15.95
$Q_{\rm B}$	55.64	435.6	~14.64
$\tilde{Q}_{\rm H}$	478.1	~152.8	21.18
$Q_{\rm a}$	27.27	414.7	8.03

Note that in the figure  $Q_{\rm H}$  is plotted for  $H_{\rm a} = 10$ , from which above  $a_{\rm H}$ ,  $b_{\rm H}$  and  $c_{\rm H}$  are determined. Accordingly these values should be multiplied by  $\eta =$ 0.5, 1.0 and 1.5 for  $H_a = 5$ , 10, and 15, respectively.

Combining Eqs.(3) and (4), we obtain

$$E_{s}(X) = \sum_{n} a_{n} p_{n} + \frac{\sum_{n} b_{n} P_{n}}{X} + \frac{\sum_{n} c_{n} P_{n}}{X^{2}} \quad (5)$$

Here, we assume the following reduction of solar radiation,

$$E_{s}(X) = E_{s0} \left( 1 - \frac{\alpha_{s1}}{X} + \frac{\alpha_{s2}}{X^2} \right)$$
(6)

Then, Eq.(5) leads

$$E_{s0} = \sum_{n} a_n p_n , \qquad (7-a)$$

$$\alpha_{s1} = -\frac{\sum_{n} b_{n} p_{n}}{E_{s0}} \quad \alpha_{s2} = \frac{\sum_{n} c_{n} P_{n}}{E_{s0}}$$
(7-b)

Let's consider  $E_{s0}$  of Eq.(7-a). Inserting numerical values of  $a_n$  and  $P_n$  at  $H_a = 5$ , 10 and 15

and y = 1, we obtain  $E_{s0} = 1182$ , 1684 and 2187  $W/m^2$  respectively. Thus,  $E_{s0}$  differs much at different  $H_{\rm a}$ . Note that  $E_{\rm s0}$  should be equal to the solar constant 1373 W/m<sup>2</sup>, for which  $H_a = 7.0$  is obtained. At the same time, y = 1.048 is determined as explained above. Then, inserting numerical values of  $b_n c_n$  and  $P_{\rm n}$  in Eq.(7-b), we obtain  $\alpha_{\rm s1} = 0.425$  and  $\alpha_{\rm s2} = 0.061$ . Note that  $E_s(X)$  can be expressed as

$$E_{s}(X) = E_{s0} \exp(-\frac{\alpha_{s1}}{X}) \approx E_{s0} (1 - \frac{\alpha_{s1}}{X} + \frac{\alpha_{s1}^{2}}{2X^{2}})$$
(8)

We have  $\alpha_{s1}^{2}/2 = 0.090$ , which is somewhat larger than the above  $\alpha_{s2}$ . However, the graphs of  $E_s =$  $E_{s0} \exp(\alpha_{s1}/X)$  and Eq.(6) against 1/X are very close to each other in the range  $1/X = 1 \sim 3$ , or  $\Theta = 90^{\circ} \sim 19^{\circ}$ .

Finally, we consider the term  $E_{sc} + Q_{IR}$ explicitly in the case of the shaded area measurement. The measured temperatures  $T_A$ ,  $T_B$  and  $T_a$  decrease as the time. This is ascribed to the decrease of  $E_{sc}$  as the solar altitude  $\Theta$ , while  $Q_{\rm IR}$  is nearly constant in daytime. Similarly to  $E_s(X)$ , we assume the following X dependence of  $E_{\rm sc}$ ,

$$E_{sc}(X) = E_{sc0} \left( 1 - \frac{\alpha_{sc1}}{X} + \frac{\alpha_{sc2}}{X^2} \right)$$
(9)

where  $E_{sc0}$ ,  $\alpha_{sc1}$  and  $\alpha_{sc2}$  are to be determined. Expanding  $Q_A$ ,  $Q_B$  and  $Q_H$  of experimental data against 1/X (see Fig.5), the coefficients for  $Q_n = e_n - e_n$  $f_{\rm n}/X + g_{\rm n}/X^2$  are obtained as follows,

Note that  $Q_{\rm H}$  in Fig.5 are expressed for  $H_{\rm a}$  = 100, so that  $e_{\rm H}$ ,  $f_{\rm H}$  and  $g_{\rm H}$  should be multiplied by 0.070 for  $H_a = 7.0$ . Taking into account Eq.(1), we have



Fig.5. Radiation energy  $Q_A$ ,  $Q_B$ , and  $Q_H$  measured in the shaded area against 1/X (=1/sin $\Theta$ ), which are fitted by  $Q_n = e_n - f_n / X + g_n / X^2$ .

$$E_{sc0} = \sum_{n=A,B,H} e_n p_n - Q_{IR}, \quad (10\text{-a})$$
$$\alpha_{sc1} = -\frac{\sum_{n=A,B,H} f_n p_n}{E_{sc0}} \quad \alpha_{sc2} = \frac{\sum_n g_n P_n}{E_{sc0}} \quad (10\text{-b})$$

Assuming  $Q_{IR} = 270 \text{ W/m}^2$  (see **Table 1**), we obtain  $E_{sc0} = 296 \text{ W/m}^2$  from Eq.(10-a). In addition, we obtain  $\alpha_{sc1} = 0.224$  and  $\alpha_{sc2} = 0.037$  from Eq.(10-b).  $E_{sc}(X)$  is expressed as

$$E_{sc}(X) = E_{sc0} \exp(-\frac{\alpha_{sc1}}{X}) \approx E_{s0} (1 - \frac{\alpha_{sc1}}{X} + \frac{\alpha_{sc1}^{2}}{2X^{2}})$$
(11)

Then, we have  $\alpha_{sc1}^2/2 = 0.025$ , which is slightly smaller than  $\alpha_{sc2}$ .

#### 4. Discussion

Here, we consider the reason of reduction factor  $\Gamma(X) = \exp(\alpha_{s1}X)$  of the solar radiation. It is known that the pressure of atmosphere decreases as the height, *z*, from the earth surface, so that the atmosphere density is expressed as

$$\rho(z) = \rho_0 \exp(-\mu z) \tag{12}$$

with  $\rho_0 = 1.526 \text{ kg/m}^3$  and  $\mu = 0.1445 \times 10^3 \text{ 1/m}$  in the standard state of  $P_0 = 1$  atm and  $T_a = 15$  °C. The sunshine is scattered and absorbed by various molecules and aerosols in the atmosphere during the pass, which is proportional to the density. Accordingly, the solar radiation varies as

$$\frac{dE_s}{dZ_p} = -\beta E_s \rho_0 \exp(-\mu Z_p \sin \Theta) \quad (13)$$

where  $Z_p (\approx z/\sin \Theta$  for  $\Theta > 20^\circ)$  is the pass length of the sunshine (see **Fig.6**), and  $\beta$  is a constant to be determined. Integrating for  $Z_p = 0 \sim \infty$ , we obtain the following relation at the earth surface,

$$E_s(\Theta) = E_{s0} \exp(-\frac{\beta \rho_0}{\mu \sin \Theta})$$
(14)

Comparing with Eq.(8), we have  $\alpha_{s1} = \beta \rho_0 / \mu$ , and  $\beta = 4.0 \times 10^{-5} \text{ m}^2/\text{kg}$  for  $\alpha_{s1} = 0.425$ . This  $\beta$  is approximately expressed as  $\beta \approx \sigma_t / M_m$  for a constant cross section  $\sigma_t$  and molecular weight  $M_m$ .

It is known, however, that the reduction process is very complicated. It is reduced by the Rayleigh scattering due to the air molecules  $N_2$  and  $O_2$ , by the absorption due to trace gases such as ozone,  $H_2O$ ,  $CO_2$ ,  $CH_4$ , etc, and by the Mie scattering and absorption due to aerosols such as vapor-water and micro-dust.

In Ref.10, the Rayleigh scattering of the solar radiation is discussed in detail. The scattering is effective in the case that the molecular size is smaller than the wavelength. The cross section depends much on the wavelength, and as shown in Ref.10, we obtain a similar expression of the reduction as Eq.(8) with  $\alpha_s = 0.108$  for  $E_{s0} = 1373$  W/m<sup>2</sup>.

Since the solar radiation is further absorbed and scattered, by the gases and aerosols, atmosphere muddiness (turbidity) factor  $R_{mud}$  is conveniently multiplied to the cross section. Then,  $\alpha_s$  is increased to 0.300, 0.412 and 0.434 with  $R_{mud} = 5$ , 9 and 10, respectively, so that  $R_{mud} = 9.5$  is appropriate. The definition of coefficient  $R_{mud}$  is similar to the coefficient  $\tau_0$  given in Table 1 (the definition is given in Ref.10).

The scattered radiation by the Rayleigh process, also discussed in Ref.10, can be expressed similarly as Eq.(11) with  $E_{sc0} = 64 \text{ W/m}^2$  and  $\alpha_{sc} = 0.40$  for  $R_{mud} = 1$ . It is imagined that the scattered radiation arrives at the earth surface through a more complicated process, so that two muddiness factors are assumed;  $R_{mudA}$  is multiplied to the cross section for the scattering in the initial process before the scattering, and  $R_{mudB}$  is multiplied to the one for the relevant scattering. Then, we obtain  $R_{mudA} = 0.25$  and  $R_{mudB} = 3.5$  as the most probable values for the experimental values  $E_{sc0} = 296 \text{ W/m}^2$  and  $\alpha_{sc} = 0.224$ .

It is required to consider the Mie scattering by aerosols, which is effective in the case when the sol size is nearly the same as the sunshine wavelength. However, it is very complicated and requires detailed information of aerosols.

As shown with Eqs.(8) and (11), the present results on  $E_{\rm s}$  and  $E_{\rm sc}$  are expressed as a function of  $\Theta$ , or the sun altitude, so that the these expressions can be applied to any case of all seasons if similar fine calm days are assumed. Then,  $E_{\rm s}$  and  $E_{\rm sc}$  at  $\Theta = 55^{\circ}$  are estimated and compared with the data given in **Table 1**. The solar radiation is  $E_{\rm s} = 817 \text{ W/m}^2$  with the muddiness factor  $R_{\rm mud} = 9.5$ , compared with  $E_{\rm s} \approx 800 \text{ W/m}^2$  and  $\tau_0 \approx 5$  at Tsukuba.



**Fig.6.** Relation of the height, z, in the atmosphere, and pass length,  $Z_p$ , of sunshine at the experimental point on the earth surface.  $\Theta$  is the sun altitude from the horizontal plain.

Similarly, the scattered radiation is  $E_{\rm sc} = 225$  W/m<sup>2</sup>, compared with  $E_{\rm sc} \approx 200$  W/m<sup>2</sup> at Tsukuba. We see the both values are fairly close to each other except for  $R_{\rm mud}$  and  $\tau_0$ . For more detailed comparison, it is necessary to make the both measurements on a fine calm day at the same time at the same place.

In conclusion, the initial purpose of this study described in section 1 was nearly achieved, but not very satisfactorily in regard to the accuracy. The present experiment on the solar and atmosphere radiations was performed with a new experimental set-up of double copper plate structure. The set-up has no glass window, and the analytical algorism of experimental data was clearly described using radiation transfer scheme, which is different from the conventional one. It is noteworthy that in spite of simple set-up and measurements the present results are not much different from the conventional ones. However, we cannot make detailed comparison between them since the measurement is not very accurate and the measured conditions are not the same. It is required to improve the experimental set-up and measurement conditions for more precise measurements.

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**Note added in proof**; The results of this work was applied to the following paper "Investigation of measures against hot summer for energy reduction and temperature stabilization in the New SUBARU experimental building" [11].

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## Numerical Study on the Rayleigh Scattering of Solar Radiation

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#### Abstract

The solar radiation from the sun to the earth decreases when passing through the atmosphere. The reduction is numerically calculated assuming Rayleigh scattering by the atmosphere molecules. For further reduction of the radiation by the scattering and absorption due to aerozoles and others, Linke's muddiness factor is introduced. Similarly, the scattered radiations by the Rayleigh's process and others are also discussed.

#### 1. Introduction

Experimental results of solar and scattered radiations were given in Ref.1, which is discussed theoretically in the present work. The solar radiation is scattered by the molecules such as N<sub>2</sub> and O<sub>2</sub> in the atmosphere when passing through the atmosphere. The scattering cross section by the molecules is given by the Rayleigh's formula, which depends on the refraction index and density of atmosphere. The density  $\rho$  [kg/m<sup>3</sup>] as well as pressure *P* [hP] and temperature *T* [K] of the atmosphere vary as the height *z* [m] from the earth surface, which are approximately expressed in the range  $z = 0 \sim z_{max}$  (= 20 km) as

$$P = 1013 \exp(-0.14467 \times 10^{-3} z)$$
(1-a)  

$$T = 289.45 - 8.9278 \times 10^{-3} z + 0.25937 \times 10^{-3} z^{-3} z^{-$$

The number density of air molecules is given by  $N(z) = \rho z/M_{\rm m}$ , where  $M_{\rm m} = 28.8 \times 10^{-3} m_{\rm p}$  with  $m_{\rm p}$  the proton mass.

The refraction index  $n (= 1 + \Delta n)$  depends on the wavelength  $\lambda(\mu m)$ , being given by [2]

$$\Delta n(\lambda, z) = \frac{C}{10^8} \frac{P(1+PG)}{T} (1-0.16\frac{HP_{\nu}}{P})$$

$$C(\lambda) = 2371.34 + \frac{683939.7}{130 - \lambda^{-2}} + \frac{4547.3}{38.9 - \lambda^{-2}}$$

$$(2-a)$$

$$(2-a)$$

$$(2-b)$$

$$G(T) = 57.9 \times 10^{-8} - \frac{9.325 \times 10^{-4}}{T} + \frac{0.25844}{T^2}$$

(2-c)

where  $H \approx 0.5$  assumed) is the humidity and  $P_v[hP]$  is the saturated vapor pressure, given by

$$P_{\nu}(T_{C}) = 6.11 \times 10^{\frac{7.5T_{C}}{T_{C} + 237.3}}$$
(2-d)

with  $T_{\rm C} = T({\rm K}) 273.2$ .

#### 2. Reduction of solar radiation

The cross section of Rayleigh scattering depends on the scattering angle  $\psi$  as  $F_{\rm R}(\psi) = (2/3)(1+\cos^2\tilde{\psi})$ . For simplicity, however, we assume isotropic scattering, with the following total cross section [3],

$$\sigma_{R}(\lambda, z) = \frac{2}{3\pi} \frac{k^{4} \Delta n}{N(z)^{2}}$$
(3)

where  $k = 2\pi/\lambda$ . Taking into account Eq.(14) of Ref.1, we have the following reduction factor of the solar radiation,

$$F(\lambda,\Theta) = \exp\left[-\int_{0}^{z_{\max}} \frac{N(z)\sigma_{R}(\lambda,z)}{\sin\Theta} dz\right] \quad (4)$$

Because of the  $k^4$  dependence of  $\sigma_{\rm R}(\lambda,z)$ , shorter wavelengths are much more scattered.

Meanwhile, the solar radiation is regarded as the blackbody radiation at temperature  $T_s = 5780$  K at the sun surface, and the spectrum outside the earth atmosphere is given by

$$u(\lambda)d\lambda = \frac{\Pi \delta \lambda}{\lambda^{5}[\exp(\alpha_{0} / \lambda T_{s}) - 1]} \quad (5)$$

where  $\alpha_0 = hc/k_B$  and  $\Pi = 2\pi hc^2 \gamma$  with  $\gamma = (R_s/D_{es})^2$ ; *h*, *c*,  $k_B$  are conventional, and  $R_s = 6.969 \times 10^8$  m the sun radius and  $D_{es} = 1.496 \times 10^8$  m the distance between the earth and the sun. The spectrum spreads out in the range  $\lambda = 0.3 \sim 3$  µm. Numerical integration of  $u(\lambda)$  over  $\lambda$  agrees with the solar energy outside the atmosphere;  $E_{s0} = \gamma \sigma_0 T_s^4 = 1373$  W/m<sup>2</sup>.

Then, the solar energy at the earth surface is calculated by

$$E_{s}(\Theta) = \int_{0}^{\lambda_{\max}} u(\lambda) F(\lambda, \Theta) d\lambda \qquad (6)$$

By numerical integration at several  $\Theta$ 's, we obtain  $E_{\rm s}(\Theta)$ , from which we obtain  $\alpha_{\rm s}=0.115 \sim 0.081$  in the range  $\Theta = 90 \sim 20$ ° for the expression  $E_{\rm s}(\Theta) = E_{\rm s0}^* \exp(\alpha_{\rm s}/\sin\Theta)$  with  $E_{\rm s0} = 1373$  W/m<sup>2</sup>. Especially, we have  $\alpha_{\rm s} = 0.108$  at  $\Theta = 55^{\circ}$ . This is very small compared with the experimental result of  $\alpha_{\rm s1} = 0.425$  at  $\Theta = 55^{\circ}$  [1].

The solar radiation, being additionally absorbed

and scattered by gases and aerosols, is further reduced. After Linke, this reduction is taken into account by multiplying atmosphere muddiness factor  $R_{mud}$  to the cross section  $\sigma_{R}$ . Then,  $\alpha_{s}$  at  $\Theta = 55^{\circ}$  is increased to 0.300, 0.412 and 0.434 with  $R_{mud} = 5$ , 9 and 10, respectively. Accordingly,  $R_{mud} = 9.5$  is the optimum.

Linke's definition of the reduction factor  $\tau_{G}$  is expressed as

$$E_s = E_{s0} \exp\left(-\frac{P}{P_0} L_R \tau_G m\right)$$
(7-a)  
$$\tau_G = 1 + \frac{L_g + L_a}{L_R} \frac{P_0}{P}$$
(7-b)  
$$m = \frac{1}{\sin \Theta} \frac{1}{\sqrt{1 + (1/35)(1/\sin^2 \Theta)}}$$

where  $L_{\rm R}$  is the optical length at m = 1 for Rayleigh scattering at the standard state (with pressure  $P_0$ ),  $L_{\rm g}$ and  $L_{\rm a}$  are the optical length for gas absorption, and for aerosol scattering and absorption, respectively. Note that  $m \cong 1/\sin \Theta$ . This  $\tau_{\rm G}$  is determined using measured  $E_{\rm s}$  and P together with calculated  $L_{\rm R}$ . We see that there is a relation of  $\tau_{\rm G}L_{\rm R} \approx \alpha_{\rm s}$ . Note that  $\tau_{\rm G}$  is further modified to  $\tau_{\rm 0}$  as follows, so that  $\tau_{\rm 0}$  is close to  $\tau_{\rm G}$ .

$$\tau_0 = 1 + (\tau_G - 1) \frac{P}{P_0} \frac{L_R(m=1)}{L_R(m)}$$
(8)

#### 3. Scattered radiation

Next, we consider the scattered radiation using the Rayleigh's isotropic cross section. Supposes that the solar radiation comes from the y direction at the solar altitude  $\Theta$ , and collides with a molecule at a point of  $(r, z, \phi)$  in the cylindrical coordinate with a distance  $d = (r^{2} + z^{2})^{0.5}$  from the origin (see **Fig.1**). The total scattered radiation arriving at the origin, normal to the horizontal plane, can be calculated-by,



**Fig.1.** Rayleigh scattering of sunshine in the cylindrical coordinate on the earth surface, representing isotropic and elliptical distributions of scattered radiation. The sunshine comes in the y direction at sun altitude  $\Theta$ .

$$E_{sc}(\lambda,\Theta) = \int_{0}^{2\pi} \int_{1}^{z_{max}} \int_{1}^{r_{max}} \frac{N(z)R_{mudB}\sigma_{R}(\lambda,z)u(\lambda)}{4\pi d^{2}} \frac{z}{d} \times \Gamma_{s}(z,\Theta)rdrdzd\phi \qquad (9)$$

where  $\Gamma_{s}(z, \Theta)$  represents the reduction factor of initial solar radiation at *z*, given by

$$\Gamma_s(z,\Theta) = \exp\left[-\frac{\langle \alpha_{inj} \rangle (z_{\max} - z)}{\sin \Theta}\right]..(10)$$

To save CPU time, the average  $\langle \alpha_{inj} \rangle$  for  $\alpha(\lambda, z) = N(z)R_{mudA}\sigma_{R}(\lambda, z)$  is introduced as,

$$<\alpha_{inj}(\lambda,z) >= \sum_{k=1}^{k_{\max}} \left(\frac{1}{k_{\max}}\right)$$
$$\times \alpha[\lambda, \frac{(k_{\max}-k)z + (k-1)z_{\max}}{k_{\max}-1}] \quad (11)$$

Here we have assumed atmosphere muddiness factors  $R_{\text{mudA}}$  and  $R_{\text{mudB}}$  for the initial radiation and scattered radiation, respectively. Integrating numerically, we obtain  $E_{\text{sc}}(\lambda,\Theta)$ . Finally, summing up over  $\lambda$  at several  $\Theta \square \text{s}$  and applying the form of  $E_{\text{sc}}(\Theta) = E_{\text{sc0}} \exp(\alpha_{\text{sc}}/\sin\Theta)$ , we obtain  $E_{\text{sc0}} = 64 \text{ W/m}^2$  and  $\alpha_{\text{sc}} = 0.40$  for  $R_{\text{mudA}} = R_{\text{mudB}} = 1$ . Experimentally, we have  $E_{\text{sc0}} = 296 \text{ W/m}^2$  and  $\alpha_{\text{sc1}} = 0.224$ , which can be fitted by  $R_{\text{mudA}} = 0.25$  and  $R_{\text{mudB}} = 4$ .

Meanwhile, there is another possibility of  $\Theta$  dependence of  $E_{\rm sc}$ . Let's consider the angular dependence  $F_{\rm R}(\psi) = (2/3)(1+\cos^2\psi)$  of the scattering without reduction of initial radiation before scattering. In **Fig.1**, the directions of initial radiation and scattered radiation toward the origin are expressed as  $n_{\rm s} = \cos \Theta \sin \Theta$ ) and  $n_{\rm sc} = (\sin \theta \cos \phi, \sin \theta \sin \phi, \cos \theta)$ , respectively, so that the scattering angle is given by

$$\cos\psi = \cos\Theta\sin\theta\sin\phi + \sin\Theta\cos\theta \quad (12)$$

When, the cross section of scattered radiation is multiplied by  $R_{\text{mudC}} = 3.5$ , we obtain  $E_{\text{sc0}} = 316 \text{ W/m}^2$  and  $\alpha_{\text{sc}} = 0.054$ , which is, however, very small compared with  $\alpha_{\text{sc1}} = 0.224$ . Thus, the effect of  $F_{\text{R}}(\psi)$  is negligible.

Above values are nearly saturated for  $r_{\text{max}} = z_{\text{max}}$ = 20 km and  $k_{\text{max}} = 5$ . It is confirmed that the spectrum of scattered radiation represents narrow peaks around  $\lambda = 0.4 \ \mu\text{m}$ , agreeing with the blue sky. It is also confirmed that the peak spectrum of solar radiation shifts from  $\lambda = 0.5 \ \mu\text{m}$  at  $\Theta = 90^{\circ}$  to 0.75  $\mu\text{m}$  at  $\Theta =$ 10°, as we see the red sun at sunrise and sunset.

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## Geometric Luminosity for the Angled Collision of Asymmetric Beams with Hourglass Effect

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#### Abstract

The geometric luminosity of angled collision of asymmetric beams with different Gaussian distributions is given in a compact formula.

Recently, we have discussed geometric luminosity of angled collision of strongly focused beams with different Gaussian distributions [1]. To treat the hourglass effect naturally, we have introduced a pseudo-isotropic beam model, in which the trajectories of colliding particles are curved similarly to the beam size variation along the propagation axis (see **Fig.1**), where the collision conditions of particles  $P_1$  and  $P_2$  are clearly determined. At a horizontal collision angle of  $2\phi$ , the reduction factor of the luminosity against the head-on collision can be expressed as

$$R_{ACHG} = \frac{\cos\phi}{\sqrt{\pi < \sigma_z^2 > -\infty}} \int_{-\infty}^{\infty} \frac{\exp(-hZ_c^2)}{\sqrt{1 + V_x Z_c^2} \sqrt{1 + V_y Z_c^2}} dZ_c$$
(1)
$$V_{x,y} = \frac{}{<\sigma_{x,y}^{*2}>}, \qquad = \frac{\frac{\sigma_{1x}^{*2}}{\beta_{1x}^{*2}} + \frac{\sigma_{2x}^{*2}}{\beta_{2x}^{*2}}}{2},$$

$$h = \frac{\cos^2\phi}{<\sigma_z^2 >} \left[1 + \frac{<\sigma_z^2 > \tan^2\phi}{<\sigma_x^{*2} > (1 + V_x Z_c^2)}\right],$$

where  $\sigma_{ix}^*$  and  $\beta_{ix}^*$  are the *i*-th horizontal beam size and beta function at the center of collision point,  $\sigma_z$  is the bunch length, the symbol <> denotes the average of colliding beams, and  $\langle U_y^2 \rangle$  is similar to  $\langle U_x^2 \rangle$ . This equation, fairly precise, can be applied to any cases of synchronous angled collision of asymmetric beams which strongly focused.

Numerical estimation of Eq.(1) is rather easy today with the aid of conventional computer, but for simplicity, we try to express it in a compact formula.

Changing the variable from  $Z_c$  to t, we have

$$R_{ACHG} = \frac{1}{\sqrt{\pi}} \int_{-\infty}^{\infty} \frac{\exp\left\{-\left[1 + \frac{\langle \sigma_z^2 \rangle}{\langle \sigma_x^{*2} \rangle} \frac{tan^2 \phi}{(1 + W_{xz}t^2)}\right]t^2\right\}}{\sqrt{1 + W_{xz}t^2} \sqrt{1 + W_{yz}t^2}} dt$$
(2)
$$W_{xz} = V_x \frac{\langle \sigma_z^2 \rangle}{\cos^2 \phi}, \qquad W_{yz} = V_y \frac{\langle \sigma_z^2 \rangle}{\cos^2 \phi}.$$

Let's make the following approximations. First, in the exponential term we assume  $1 + W_{xz}t^2 \approx 1$ since it is observed in numerical examples that  $R_{ACHG}$  is little affected by this term. Second, the denominator is assumed as

$$\sqrt{1+W_{xz}t^2}\sqrt{1+W_{yz}t^2} \approx \sqrt{1+Wt^2}$$

with  $W = W_{xz} + W_{yz}$ . Then, Eq.(2) is expressed as



**Fig.1.** Angled collision of asymmetric beams at a horizontal crossing angle  $2\phi$ . Trajectories of particles  $P_1$  and  $P_2$  are curved similarly to the beam size variation along the propagation axis and collide at Q.

$$R_{ACHG}^* \approx \frac{1}{\sqrt{\pi}\sqrt{A}} \int_{-\infty}^{\infty} \frac{\exp(-s^2)}{\sqrt{1+Bs^2}} ds, \qquad (3)$$

$$A = 1 + \frac{\langle \sigma_z^2 \rangle}{\langle \sigma_x^{*2} \rangle} tan^2 \phi, \qquad B = \frac{W}{A}.$$

If  $W_{xz} \ll 1$ , then  $R^*_{ACHG}$  is very close to  $R_{ACHG}$ . Meanwhile, the integral of Eq.(3) has been considered in Ref.[2], and expressed as

$$R_{ACHG}^* \approx \frac{1}{\sqrt{\pi}\sqrt{AB}} \exp(\frac{1}{2B}) K_0(\frac{1}{2B}), \quad (4)$$

where  $K_0$  is the modified Bessel function of order zero.

**Figure 2** shows numerical examples of  $\phi$  dependence of reduction factors  $R_{ACHG}$  of Eq.(1) and  $R_{ACHG}^*$  of Eq.(4) for the  $e^{\mp}e$  collision in PEP II and for a tentative laser-electron beam collision, parameters of which are given in Ref.[1]. It is observed that factors  $R_{ACHG}$  and  $R_{ACHG}^*$  agree very well in both cases, but there is a slight difference in the case of laser-electron beam collision. This is because  $W_{xz}$  is negligibly small in the former case but not in the latter case, as indicated in the figure.

In a special case of symmetric beams, horizontally flat and vertically focused, we have  $W_{xz} \ll 1$  and  $W \approx (\sigma_z / \beta_y)^2$ . Then,  $R_{ACHG}^*$  is reduced to an existing formula [3].



Fig. 2. Angle dependences of reduction factors  $R_{ACHG}$  and  $R_{ACHG}^*$  are shown for the cases of  $e^+e$  collision of PEP II and for a tentative laser-electron collision. In the figure,  $\phi_t$  is the transition angle, above which the hourglass effect becomes less effective.

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## **Observation of Smith-Purcell radiation in Terahertz** regime at electron linear accelerator LEENA

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#### Abstract

Terahertz radiation by the Smith-Purcell effect was successfully observed using 15 MeV electron beams of the linear accelerator LEENA. The radiation properties such as the angular dependence of peak wavelength were measured. Wavelength spectrum measured by the Martin-Puplett interferometer is very clear and the peak wavelength well corresponds to the calculated one.

#### Introduction

In order to develop high peak power, wide range (0.1-10 THz) and tunable terahertz radiation sources using relativistic electron beams, we have been upgrading the compact electron linear accelerator LEENA [1-5]. The electron beams with bunch length shorter than the wavelength of emitted light can generate high power radiation by coherent radiation. The main parameters of LEENA are shown in Table. I. In addition to the synchrotron radiation from a bending magnet, the Smith-Purcell radiation from a metal grating plate near an electron orbit was successfully observed. The spectrum of Smith-Purcell radiation was measured with the Martin-Puplett interferometer. In this paper we report the present status of the Smith-Purcell radiation in a terahertz regime.



Fig.1 Observation of Terahertz radiation using LEENA electron beams; synchrotron radiation and Smith-Purcell radiation.

#### **Experimental results of Smith-Purcell radiation**

The copper plate with grating period of 10 mm is equipped in a vacuum chamber of the LEENA. Using three mirrors located in the chamber, terahertz radiation can be extracted into the air through a quartz viewport. The Smith-Purcell radiation in a terahertz regime was measured with a Zero Bias Detector. Measured radiation power is about ten micro Watt. Because present bunch length is longer than terahertz

wavelength, the measured radiation is incoherent. The emitted wavelength of Smith-Purcell radiation has an angular dependence, i.e., shorter wavelength light is radiated in the forward direction and longer wavelength in the backward direction. The mirrors in the chamber can rotate according to the desired angle for measurement. Fig. 2 shows the angular dependence of radiation power measured by the two detectors with different measurement ranges. The calculated emission angle for the light of 0.075-0.11 THz is about 40 degrees and for 0.11-0.17 about THz 50 degrees. Experimental results show a good agreement to the calculation.



Fig.2 Observation of angular distribution of Two detectors Smith-Purcell radiation power. with different measurement ranges are used: 0.11-0.17 THz (upper) and 0.075-0.11 THz (lower).

Table I Main parameters of LEENA.

Beam energy	6-15 [MeV]
Macropulse current	100 [mA]
Macropulse width	5 [us]
Repetition frequency	10 [Hz]
Gun	RF gun
Cathode	LaB <sub>c</sub> (thermal)
Bunch length	~30 [ps]

#### Smith-Purcell radiation spectrum measured by Martin-Puplett interferometer

In a terahertz regime, the wire grid reflects the radiation component whose direction of the polarization plane is parallel to the wire and transmits the perpendicular component. The Martin-Puplett interferometer uses wire grids as a divider of terahertz light as shown in Fig. 3. The interferogram made from a path length difference between two lights by moving a mirror was measured with a ZBD. By the Fourier transform of this interferogram data, the wavelength spectrum of Smith-Purcell light is obtained as shown in Fig.4. Measured peak wavelength of Smith-Purcell light is 3.4 mm and is well corresponding to the calculations.



Fig.3 Martin-Puplett Interferometer



Fig.4 Interferogram of Smith-Purcell radiation measured with Martin-Puplett interferometer (left) and its FFT result (right).

#### Summary and Future plan

The Smith-Purcell light was successfully observed at LEENA accelerator. The observed terahertz radiation is incoherent, that is the electron bunch length is longer than the light wavelength. If the bunch length becomes shorter than the light wavelength, coherent radiation occurs and radiation intensity becomes several orders higher. To make electron bunch shorter using an alpha magnet effectively, new solenoid coil is under construction just after the electron gun to suppress beam divergence. The emission angle of coherent Smith-Purcell (CSP) radiation depends on the electron bunch length. Thus CSP is not only a powerful terahertz light source but also a useful beam monitor for electron bunch length in linear accelerators.

And the construction of new terahertz beam-line for user experiments will be started in the summer of 2013.

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## Energy calibration of electron beams by laser Comptonscattering γ-rays at BL01

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#### Abstract

We have calibrated electron beam energies in a nominal energy range 550 - 974 MeV using laser-Compton scattering  $\gamma$ -ray beams at the synchrotron radiation facility NewSUBARU. The  $\gamma$ -ray beams were produced at energies from 562 keV to 1727 keV and detected with a high-purity germanium detector. The electron beam energies were determined by reproducing the full energy peaks of the  $\gamma$ -ray beams by Monte Carlo simulations with a precision of 0.068% in 1 $\sigma$ .

#### Introduction

In the NewSUBARU, electrons are injected from a linear accelerator into a storage ring and undergo a top-up operation at the nominal energy 974 MeV. The storage electrons can be either accelerated up to 1.5 GeV or decelerated down to 0.5 GeV. Recently, a new y-ray experimental hutch, GACKO (Gamma Collaboration Hutch of Konan University), was built at NewSUBARU-BL01 and has become fully operational. Quasi-monochromatic  $\gamma$ -ray beams can be produced in the energy range 1 - 76 MeV by the laser Compton scattering. The capability of tuning the electron beam energy between 0.5 GeV and 1.5 GeV is important to nuclear physicists who use the laser Compton scattering (LCS)  $\gamma$ -ray beams [1, 2]. However, the nominal energy of electrons is determined only with 1% uncertainty based on the beam optics of the storage ring [3].

We calibrated the electron beam energy by producing low-energy LCS  $\gamma$ -ray beams with a CO<sub>2</sub> laser, where  $\gamma$ -ray energies are in the range of the standard  $\gamma$ -ray sources. This report presents the energy calibration for electron beams stored in a storage ring NewSUBARU at nominal energies between 550 MeV and 974 MeV. The absolute calibration of the electron beam offers an opportunity to calibrate the energy of LCS  $\gamma$ -ray beams.

#### **Experiments and Results**

Low-energy LCS y-ray beams were produced below 2 MeV with a grating-fixed CO<sub>2</sub> laser (wave length  $\lambda$ =10.59 µm). Electrons were injected from a linear accelerator into the NewSUBARU storage ring at the nominal energy 974 MeV, decelerated to 950 MeV, and sub- sequently down to 550 MeV in steps of 50 MeV. The LCS y-ray beams were measured with a coaxial (64 mm in diameter  $\times$  60 mm in length) high-purity germanium detector (HPGe). The energy of  $\gamma$ -ray spectra was calibrated with the standard  $\gamma$ -ray sources, 60Co including the sum peak, 133Ba, 137Cs, and 152Eu and a natural radioactivity 40K. The energy calibration was carried out before and after the measurement of LCSy-rays. From the calibrated  $\gamma$ -ray spectra, we determined absolute values of the electron beam energies by means of Monte Carlo simulations in a nominal energy (Ee<sup>n</sup>) range 550 - 974 MeV.

Figure 1 shows results of the energy calibration for the HPGe detector carried out before the measurement of LCS  $\gamma$ -ray beam. The best linear fit to the data gives a relation between the  $\gamma$ -ray energy  $E\gamma$  in keV and the channel number X by  $E_{\gamma}$  = 0.3624X-0.8022. The data taken after the LCS  $\gamma$ -ray measurement gives the same slope coefficient and an intercept -0.7458. The uncertainty of the energy calibration is 0.08% in  $1\sigma$  in the energy range 120 keV - 2.5 MeV. The electron beam energy was determined by Monte Carlo simulations that best reproduce the experimental  $\gamma$ -ray spectra measured with the HPGe detector. The simulation code incorporates the production process of  $\gamma$  rays in the inverse Compton scattering into the EGS4 code [4] which simulates interactions of photons with the detector material.

The energy of the LCS  $\gamma$  rays is given by

$$E_{\gamma} = \frac{4\gamma^2 \varepsilon_L}{1 + \gamma^2 \theta^2 + 4\gamma \varepsilon_L / (mc^2)}$$
(1)

where  $\varepsilon_L$  is the energy of a laser photon,  $mc^2$  is the rest-mass energy of an electron,  $\theta$  is the scattering angle of the laser photon with respect to the electron beam, and  $\gamma$  is the Lorentz factor of the relativistic electron which is defined by  $\gamma = E_e/mc^2$  with the total electron energy  $E_e$ . For simplicity, the collision



FIG. 1. Energy calibration of the HPGe detector with the standard  $\gamma$ -ray sources. The solid line is the best linear fit to the data.
Counts

Counts

Counts

<sup>400</sup> between laser photons and electrons is assumed to take place at a point where the electron beam forms a <sup>300</sup> narrow waist in the beam optics. The collision point with a maximum collision efficiency is located at a <sup>200</sup> distance of 887cm for the GO<sub>2</sub> laser ( $\lambda$ =10.59 µm) photons from a publicator and at 1847 cm for the <sup>100</sup> Neutron laser ( $\lambda$ =1064 nm) photons [2]. The electron beam size, which is smaller than the photon beam size at the collision point, determines the size <sup>160</sup> of a light source that em<sup>105</sup>  $\gamma$  rays inside a solid angle subtended by a 2 mm (in diameter) collimator made <sup>500</sup> of 10 cm thick Pb. We introduce an effective source <sup>400</sup> size in circular shape. The (b) ctron beam spot is circular at the collision point for 10.59 µm photons of 300the CO<sub>2</sub> laser but is elliptic for 1064 nm photons of the Nd:YVO<sub>4</sub> laser [2].

Monte Carlo simulations were carried out to 200 -<sup>100</sup> reproduce the examinental  $\gamma$ -ray spectra with two fining parameters, the effective source size ( $\zeta$ ) and othe electron beam energy. It is to be noted that the <sup>1</sup>energy resolution of the HPGe detector was taken into account as ap energy spread of the electron beam 8009m the Monte Carlo simulations. The energy resolution of the HPGe detector was 6.7 keV (0.5%) 6000in full width at half maximum (FWHM) for 1332 keV  $\gamma$  rays (60Co). Following the relation ( $\Delta E_{\gamma}/E_{\gamma}$ )  $\approx$  $4002(\Delta E_e/E_e)$  based on Eq. (1), the detector resolution was incorporated thto the simulation as ( $\Delta E_e / E_e$ )  $\approx$ 2000 1% in the standard deviation of Gaussian function. Examples of the best fits to the spectra are shown in Fig. 2. The full energy peaks were well reproduced by the Monte Carlo simulations with the effective



FIG. 2. (%) Monte Carlo simulation (dotted line) with an electron beam energy  $E_e^{r}=982.2$  MeV for LCS  $\gamma$ ray spectral produced with a CO<sub>2</sub> laser in comparison with the experimental data (solid line) taken at the nominal energy  $E_e^{n}=974$  MeV, (b) The same as (a), but for a simulation with Eg = 860.7 MeV in comparison with the that at En = 850 MeV.





FIG. 3. The difference  $\Delta E$  of the real energy  $E_e^r$  from the nominal energy  $E_e^n$  of the electron beams:  $\Delta E = E_e^{r}$ - $E_e^n$ . The solid line is the 4th-order polynomial fit to the data. See text for details.

energy associated with the simulation was 0.1%. Together with the 0.08% uncertainty arising from the energy calibration, the  $\gamma$ -ray energy was determined with 0.128% uncertainty, which corresponds to 0.064% uncertainty in electron beam energy.

Figure 3 shows  $\Delta E = E_e^r - E_e^n$ , the difference of the real energy  $E_e^r$  of the electron beams thus determined by the Monte Carlo simulation from the nominal energy  $E_e^n$  as a function of  $E_e^n$ . The 4thorder polynomial fit to the data gives

$$\Delta E = -4.695 \times 10^{-10} (E_e^n)^4 + 1.302 \times 10^{-6} (E_e^n)^3 -1.360 \times 10^{-3} (E_e^n)^2 + 0.6385 (E_e^n) - 103.94$$
(2)

Here  $\Delta E$  and  $E_{e^n}$  are given in MeV.

An attempt was made of experimentally detecting the neutron threshold for Au located at 8.072 MeV [5]. A disk of 2mm-thick Au was irradiated with the LCS  $\gamma$ -ray beams produced with the Nd:YVO<sub>4</sub> laser at the not in the lectron-beam energies from 677 to 661 in steps of 2 MeV. By changing the electronbeam energy by 2 MeV, we changed the  $\frac{1}{2}$ -ray energy by ~  $\mathfrak{D}$  keV. Neutrons were detected with a  $4\pi$  triplering feution detector [6]. Statistically significant eventing were observed above 667 MeV followed by no net counts at the three lowest energies, 665, 663, and 661 MeV. In view of the fact that the LCS  $\gamma$ -rays at the threshold energy for Au are produced by 676.52 MeV electron with a prominal energy of 667 (665) MeV is, in reality, harger (smaller) than 676.52 MeV. Thus, the result of the experimental detection of the neutron threshold for Au is consistent with the present energy calibration.

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# NEXAFS Study on Hyperthermal Atomic Oxygen Beam Irradiation Effect on the Ti-containing DLC Film

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## Abstract

Surface structural changes of Ti-doped diamond-like carbon (Ti-DLC) film exposed to a hyperthermal atomic oxygen beam were investigated using near-edge X-ray absorption fine structure (NEXAFS) spectroscopy using synchrotron radiation. The spectral shape of the C K NEXAFS spectrum of as-deposited Ti-DLC film resembled that of DLC film. After exposure to atomic oxygen, the spectrum resembled that of TiC powder. On the other hand, the spectral shape in the Ti L NEXAFS spectrum of as-deposited Ti-DLC film resembled that of TiC powder and became similar to that of TiO<sub>2</sub> powder after exposure to atomic oxygen. These changes are ascribable to the desorption of C atoms as CO and/or CO<sub>2</sub> from Ti-DLC film due to the irradiation of atomic oxygen beam.

## Introduction

Diamond-like carbon (DLC) films were expected to be used as lubrication materials in space, where oil cannot be used, because they exhibit excellent friction properties both in a vacuum and in air. One of the most important concerns is the reliability of DLC films as a lubricating material in an extreme space environment (temperature, soft X-ray, radiation of atomic oxygen, and their synergistic conditions). The most important factor in causing deterioration of the material in low Earth orbit (LEO), where artificial satellites and spacecraft are positioned, is atomic oxygen exposure. In this orbit, artificial satellites and spacecraft are exposed to atomic oxygen with a translation energy of 5 eV. In our previous study, we investigated the effects of atomic oxygen atomic oxygen beam source [1]. A departure of hydrogen from DLC films and structural change of carbon atom in the surface layer of a hydrogenated DLC film were verified during hyperthermal atomic oxygen exposure.

Recently, the development of functional DLC films advanced due to the incorporation of other elements, such as N, Si, F, and metal content, into DLC films to enhance their electrical, optical, and mechanical properties. In particular, Ti-doped DLC films have been widely investigated due to their thermal stability. In the present study, we investigated the effect of atomic oxygen exposure with an impinging energy of 5 eV on the surface chemistry and structure of Ti-DLC films by measuring the near-edge X-ray absorption fine structure (NEXAFS) spectra.

## **Experimental methods**

The Ti-containing hydrogenated DLC (Ti-DLC) films used in this study are commercially available. The films were deposited at 200 nm thickness on Si wafers by using an amplitude modulated RF plasma-enhanced chemical vapor deposition (CVD) method. The hydrogen content of these films were estimated to be greater than 40 at.% using the combination of Rutherford backscattering spectrometry (RBS) and elastic recoil detection analysis (ERDA) of DLC films by using the same synthesis method.

The exposure of an atomic oxygen beam into the Ti-DLC films was done using a laser detonation-type beam apparatus located at the Kobe Univ. The translational energy of atomic oxygen was estimated to be 5.46 eV by using a time-of-flight (TOF) measurement system consisting of a quadrupole mass spectrometer with a scintillation detector and a multichannel scalar. The typical atomic oxygen flux at the sample position (46 cm from the nozzle) was estimated to be  $3.51 \times 10^{15}$  atoms cm<sup>-2</sup> s<sup>-1</sup> by using a Ag-coated quartz crystal microbalance (QCM). In the present study, four sheets of Ti-DLC film were exposed to an atomic oxygen beam corresponding to the fluences of  $2.74 \times 10^{19}$ ,  $5.47 \times 10^{19}$ ,  $8.3 \times 10^{19}$ , and  $1.85 \times 10^{20}$  atoms cm<sup>-2</sup>, respectively. All exposure experiments were carried out at room temperature.

The NEXAFS measurements were carried out on beamline 09A (BL09A). Undulator light dispersed by a invalid spacing planer-grating monochromator was irradiated on the sample film at 54.7° (magic angle) with respect to the surface normal of the samples. The NEXAFS spectra were measured in the total electron yield mode. The measured energy range of the C K edge absorption and Ti L edge absorption were 275–330 eV and 450-500 eV, respectively.

## **Results and Discussion**

Figure 1 shows the C *K*-edge NEXAFS spectra of a Ti-DLC film exposed to by an atomic oxygen beam with that of a Ti-DLC film before exposure. The spectral features of the C *K* NEXAFS spectrum of the Ti-DLC film before exposure resembled that of the DLC film. By the exposure to an atomic oxygen beam, the spectral features of the C *K* NEXAFS spectrum of the Ti-DLC film noticeably changed. 1) A sharp peak was observed at 289 eV due to the increase in intensity at which a peak was observed as a small shoulder peak in the spectrum of the Ti-DLC film before exposure. 2) The intensity of the peak at 285.4 eV decreased. This decrease indicates that the  $sp^2$  component decreased in the Ti-DLC film. The spectral features of the Ti-DLC film after exposure to atomic oxygen beam resembled that of TiC powder. In addition, the peak at 289 eV was assignable to the  $1s \rightarrow \sigma^*$  transition originating from the C atoms neighboring the Ti atoms.

Figure 2 shows the Ti *L*-edge NEXAFS spectra of the Ti-DLC exposed to an atomic oxygen beam with that of the Ti-DLC film before exposure. The spectral features of the Ti *L* NEXAFS spectrum of the Ti-DLC film before exposure resembled that of TiC powder. After exposure to an atomic oxygen beam, the spectral features of the Ti-DLC films changed and became similar to those of  $TiO_2$  powder.

From these results, the changes in the local structure of the Ti-DLC film due to exposure to an atomic oxygen beam are summarized as follows: 1) In the as-deposited Ti-DLC films, almost all the C atoms were bonded to each other with single bonding and double bonding at a certain ratio. Most of the Ti atoms bonded to the C atoms. 2) After exposure to an atomic oxygen beam, most of the C atoms bonded to Ti atoms and most of the Ti atoms bonded to the O atoms. These changes are ascribable to the desorption of C atoms from Ti-DLC films due to the irradiation of the atomic oxygen beam. The C atoms were desorbed from the films as gas species (CO and/or  $CO_2$ ). On the other hand, oxidized Ti (TiO<sub>x</sub>) was not desorbed from the Ti-DLC films as a gas species. Therefore, the Ti/C ratio on the surface of the Ti-DLC films increased due to the irradiation of the atomic oxygen beam. As the result, residual C atoms bonded to the Ti atoms. The  $sp^2/(sp^2+sp^3)$  ratio of C atoms in the Ti-DLC films exponentially decreased because the C-Ti bonding could not form double bonding. The discrepancy a the previous work on DLC film [1] is ascribable to Ti-DLC films containing Ti atoms, which were not desorbed from the film even if they were oxidized due to the irradiation of an atomic oxygen beam.



Fig.1 C *K*-edge NEXAFS spectra of commercial DLC film and Ti-DLC films before and after exposure to atomic oxygen beam and TiC powder

Fig.2 Ti *L*-edge NEXAFS spectra of TiC powder, Ti-DLC films before and after exposure to atomic oxygen, and  $TiO_2$  powder.

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# Soft X-ray Irradiation Effect on Highly Hydrogenated Diamond-like Carbon Films

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#### Abstract

Surface and bulk properties' changes of a hydrogenated Diamond-like carbon (H-DLC) film exposed to synchrotron radiation (SR) in the soft X-ray region were investigated by an atomic force microscope (AFM) and a combination of Rutherford Backscattering Spectroscopy (RBS) and Elastic Recoil Detection Analysis (ERDA) techniques. The surface of H-DLC films became flat and the hydrogen content of H-DLC films decreased with increasing SR dose.

#### Introduction

Diamond-like carbon (DLC) films have excellent properties including high hardness, a low friction coefficient, high abrasion quality, a gas barrier, chemical inertness, and surface lubrication and are therefore being utilized as coating materials on automobile parts, hard disks, artificial blood vessels, edged tools, and food containers. Film-forming methods affect the properties of DLC films differently, and thus a wide variety of DLC films have been developed. DLC films are expected to be used in outer space as a lubrication substitution for oil, which cannot be used in space because it disappears in vacuums [1-2].

DLC films are generally known to be durable against X-ray exposure [3]. However, it has recently been reported that soft X-ray exposure on highly hydrogenated DLC (H-DLC) films leads to desorption of hydrogen and an increase in film density and refractive index [4-5]. A theoretical calculation has suggested that this hydrogen desorption could be associated with a structural change of DLC films [6]. Clarification of the effect of soft X-ray exposure on DLC films is necessary to ensure that DLC films can be used in outer space safely.

In this study, we investigated the modification processes by soft X-ray exposure on H-DLC films. Specifically the SR dose dependence of surface roughness (Ra), and hydrogen content was investigated. The elementary composition analysis was performed using a combination of Rutherford Backscattering Spectroscopy (RBS) and Elastic Recoil Detection Analysis (ERDA) techniques. The surface roughness was measured using an atomic force microscope (AFM).

#### **Experiments**

200-nm-thick H-DLC films were deposited on Si wafers by using an amplitude-modulated RF plasma-enhanced CVD method. This method enables the deposition of DLC films containing a lot of hydrogen. The SR irradiation of the H-DLC films was carried out at BL06 of the NewSUBARU synchrotron facility at the University of Hyogo, Japan. The SR at the BL06 sample stage had a continuous spectrum from IR to soft X-rays, lower than 1 keV. This includes 300 eV, which is the ionization energy of a carbon *K* edge. As a result, the *K*-shell electrons of the C atoms could be excited by the SR at BL06. During this experiment, the electron energy of the NewSUBARU ring was 1.0 GeV. The BL06 sample stage was room temperature and the pressure in the chamber was the order of  $10^{-5}$  Pa. An SR dose [mA+h] is derived from the product of the ring current [mA] and exposure time [h]. The exposure on the H-DLC films was carried out over SR doses ranging from 0 to 3000 mA+h.

## **Results and discussion**

The hydrogen content of H-DLC films was quantitatively determined by RBS/ERDA. The measurements were performed using an electrostatic accelerator (Nissin High Voltage, NT-1700HS) located at the Extreme Energy-Density Research Institute, Nagaoka University of Technology, Japan. He<sup>+</sup> ions accelerated to 2.5 MeV using a tandem Pelletron accelerator were used as the incident beam, whose angle with respect to the surface normal was 72°. The measurement error of this apparatus is 1%.

Figure 1 shows the SR dose dependence of the hydrogen content of H-DLC films. The hydrogen content of the unirradiated H-DLC films was  $\approx 50$  %. After SR exposure, the hydrogen content drastically decreased in the range of 0–200 mA·h, eventually becoming  $\approx 30$  % at 200 mA·h. Above  $\approx 200$  mA·h, the hydrogen content slowly decreased and consequently became  $\approx 20$  %. This result shows that the SR exposure on H-DLC films leads to hydrogen desorption. However, hydrogen of  $\approx 20\%$  in H-DLC films had no influence due to SR exposure. This indicates that hydrogen atoms exist at different chemical environments in H-DLC films: where hydrogen emitted or not emitted from films by the exposure to soft X-rays. It has previously been found that the structure of H-DLC films varied to that of typical DLC films whose hydrogen content is

20-30 % by the exposure to soft X-rays [5].

The surface roughness of the H-DLC films were measured by using a tapping method with AFM apparatus (SII nanotechnology E-sweep/nanoNavi Station); the determining area was  $1000 \times 1000$  nm. SR dose dependence of Ra estimated by the measurements of AFM, are shown in Fig. 2. The Ra of the unirradiated H-DLC films was 0.29 nm, which was the largest. The Ra of H-DLC films with even smallest SR dose (10 mA · h) rapidly decreased compared to the unirradiated one. In addition, Ra remained approximately constant at  $\approx 0.18$  nm in regions above  $\approx 100$  mA · h. These results show that SR exposure on H-DLC films led to a decrease of Ra, and it also flattened the surface of the H-DLC films. In terms of the hydrogen content, the change was observed in  $\approx 0-200$  mA · h. In contrast, the process of flattening decreased at a lower SR dose. Therefore, the process of surface flattening differs from that of hydrogen desorption.

The modification of H-DLC films by the SR exposure includes hydrogen desorption and surface flattening. Immediately after the SR exposure, the surface becomes flat due to desorption from the salient. Up to  $\approx 200 \text{ mA} \cdot \text{h}$ , the hydrogen content of the H-DLC films was  $\approx 30 \%$ .



Fig. 1. SR dose dependence of hydrogen content of H-DLC films.  $\bigcirc$  and  $\bullet$  represent unirradiated and

irradiated, respectively.

roughness of H-DLC films.  $\bigcirc$  and  $\bullet$  represent unirradiated and irradiated, respectively.

## Conclusions

Soft X-ray irradiation effect on the surface and material properties of highly hydrogenated Diamond-like carbon thin films was investigated using an atomic force microscope (AFM) and a combination of Rutherford Backscattering Spectroscopy (RBS) and Elastic Recoil Detection Analysis (ERDA) techniques. The hydrogen content of H-DLC films decreased from  $\approx 50$  % to  $\approx 20$  % by the SR exposure on films. Hydrogen desorption was not observed at higher doses. In the range of  $\approx 0-200$  mA·h, hydrogen content decreased. In contrast, the surface roughness (Ra) of the H-DLC films decreased at lower SR doses compared with hydrogen content, and the surface of the H-DLC films became flat. We found that the modification processes of H-DLC films by SR exposure include hydrogen desorption and flattening on the surface.

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# Low-Temperature Activation of Boron in Si wafer by Soft X-ray Irradiation

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### Abstract

Novel activation method of B dopant using a soft X-ray undulator was investigated. The activation energy of B activation by soft X-ray irradiation was lower than that of B activation by an annealing. As the irradiated photon energy closed with the core level of Si 2p, the activation ratio increased. This related to the enhancement of electron excitation as a base on Felmi golden rule. At low temperature, the B activation occurred by the atomic migration of Si atoms due to Coulomb force via the electron excitation.

## Introduction

Fabrication method of an ultra-shallow junction lower than 10 nm is required. We proposed a novel activation method of B dopant at low temperature by using a soft X-ray undulator [1]. The photon energy dependence of sheet resistance was investigated. In addition, the mechanism of soft X-ray activation was discussed in comparison with a conventional thermal activation.

## Exprimental

B ions were implanted to Si (100) wafer (n-type, 8-12  $\Omega$ cm) with an energy of 5 keV and a dose quantity of  $2 \times 10^{15}$  cm<sup>-2</sup>. The irradiation of soft X-ray was carried out at BL07A of NewSUBARU[1]. The photon energy was changed from 50 to 250 eV, with the dose quantity of 50 mA h. In addition, to reduce the sample temperature, the storage-ring current decreased from 250 to 50 mA. The gas pressure during irradiation was  $6 \times 10^{-5}$  Pa. The surface temperature of Si substrate during soft X-ray irradiation was measured by thermocouple and via a ZnSe window by a thermo-viewer. For the comparison, the annealing in N<sub>2</sub> atmosphere was carried out in the range of 100 to 1000°C.

The sheet resistance was measured by a four-point probe method at room temperature. The activation ratio is given by Irvin curve and dopant dose quantity. Activation energy of B activation ( $E_a$ ) was estimated by Arrhenius plot of activation ratio.

## **Results and discussion**

The sheet resistance and the temperature of Si wafer as a function of photon energy are shown in Fig. 1. The temperature at the photon energy of 100 eV, which corresponds to the energy level of Si 2p core-electron (99.8 eV), shows the highest value. The Si 2p core-electrons of Si atom are excited by soft X-ray irradiation and they relax resulting in a temperature increase of Si wafer. The activation was enhanced at 100 eV. According to Felumi golden role, the electron excitation is enhanced by closing to energy of core level. It is found that the sheet resistance after soft X-ray irradiation strongly depended on the irradiated photon energy.

As the storage ring current decreased, the sample temperature decreased to 110°C and the sheet resistance was increased to 3.1 k $\Omega/\Box$  (Fig. 2). The sheet resistance of annealed sample at 100°C was 8.0 k $\Omega/\Box$ . It shows that the activation was enhanced by the electron excitation during the soft X-ray irradiation.

The relationship between the activation ratio and the reciprocal absolute temperature are shown in Fig. 3. The sheet resistance of soft X-ray irradiated Si was lower than that of annealed Si below 400°C. The  $E_a$  for the soft X-ray activation was smaller than that for the annealing. The discrepancy of  $E_a$  between the soft X-ray irradiation and annealing indicates that the soft X-ray activation occurred by not only the thermal effect but also the excitation of the core electrons followed by the atomic migration.

The activation mechanism of B by soft X-ray irradiation is considered as follows (Fig. 4). The activation by annealing generally occurs by movement of dopant atoms to lattice sites of Si. This process corresponds to the Arrhenius plot for thermal annealing in high temperature range. The soft X-ray irradiation enhances the atomic

migration via excitation of Si2p core-electrons of Si. During the recovery of crystallinity in amorphizated Si surface by atomic migration via electron excitation, B atom can shift to the lattice site of Si atom. Because the size of B atoms is smaller than that of Si atom, the B activation is influenced by atomic migration of Si such as "knock-on" effect.

## Conclusions

1) The activation of B dopant occurs at 110°C, although the activation ratio shows small value of  $6.2 \times 10^{-3}$ . The B activation ratio of Si wafer subjected to photon with an energy of Si2p and B1s were  $1.8 \times 10^{-2}$  and  $5.7 \times 10^{-3}$ , respectively. Because the size of B atoms is smaller than that of Si atom, the enhancement of Si migration by soft X-ray irradiation triggers the movement of B atoms.

2) The B activation energy for the soft X-ray irradiation was smaller than that for the annealing. The soft X-ray activation occurred by not only the thermal effect but also the excitation of the core electrons followed by the atomic migration.

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Fig. 1. Sheet resistance (closed symbol) and temperature of Si wafer (open symbol) as a function of photon energy of soft X-ray. The insert shows the sheet resistance of Si wafer for the photon energy from 90 to 115eV.



Fig. 2. Sheet resistance and sample temperature as a function of photon flux density (storage-ring current) at photon energy of 115 eV. The B activation occurs at  $110^{\circ}$ C, although the activation ratio shows small value of  $6.2 \times 10^{-3}$ .



Fig. 3. Relationship between the activation ratio and reciprocal absolute temperature. Activation energy of B dopant activation was estimated from the slope. The  $E_a$  for the soft X-ray activation (0.06 and 0.09 eV) was smaller than that for the annealing (0.16 eV).



Fig. 4. Schematic diagram of mechanism of low-temperature activation by soft X-ray irradiation. The soft X-ray irradiation enhances the atomic migration via excitation of Si2p core-electron. During the recovery of crystallinity in amorphizated Si surface by the atomic migration via the electron excitation, B atom can shift to the lattice site of Si atom.

# Surface Modification in Silica-Based Films by Undurator Radiation

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#### Abstract

Undulator radiation (UR) by the NewSUBARU is used to modify the surface in pure silica and GeO<sub>2</sub>-doped silica films for optical waveguide devices. Irradiated films are found to show reduction for both SiO<sub>2</sub> and GeO<sub>2</sub> bonds by analyzing XPS (X-ray Photoelectron Spectroscopy) results. The surface reduction results generating Si-Si bonds show a clear peak-energy-dependence of UR, in which there is a threshold energy near the  $L_3$  absorption-edge for Si. The surface reduction layer for Si-Si bonds is found to be very thin less than 1.5nm, while that for Ge-Ge bonds is less than 40nm.

## Introduction

We use synchrotron radiation (SR) and undulator radiation (UR) for photo-induced refractive-index modifications in silica-based glasses for optical waveguide devices<sup>1,2)</sup>. Our main objectives are to induce large refractive-index changes more effectively using SR or UR without a spectrometer, and to investigate their origins depending on wavelengths of SR or UR spectra. Especially, UR would be a very useful tool for the materials modifications, because it can select a useful wavelength and it has very high intensity. For those reasons we mainly use UR for the materials modifications. In this report, we investigated the modification effects on the surface of SiO<sub>2</sub> films or GeO<sub>2</sub> doped SiO<sub>2</sub> films irradiated with UR. XPS was mainly used for the characterizations.

## **Experiments and Results**

Experimental conditions are almost the same as in the previous experiments<sup>1,2)</sup>. UR (from the NewSUBARU BL-7A) was mainly used to investigate irradiation-wavelength effects. SR (from the NewSUBARU BL6) was also irradiated on samples directly without a spectrometer. The electron energy of the SR was 1GeV. The UR peak energy in the first order was controlled from 20 to 120 eV. The samples were thermally grown SiO<sub>2</sub> films (0.5 or 1  $\mu$ m thickness) on Si substrates and GeO<sub>2</sub>-doped SiO<sub>2</sub> films (2  $\mu$ m thickness) fabricated by the FHD (Flame Hydrolysis Deposition) technique on Si substrates in this experiments. Relative refractive index difference for the GeO<sub>2</sub>-doped SiO<sub>2</sub> films was 1.9%. XPS measurements and the following RIE (Reactive Ion Etching) were used to investigate the surface reduction effects and depth profiles for the modification.

It was shown in Fig.1 that Si-Si bonds were generated on the surface of thermally grown SiO<sub>2</sub> films, after irradiating UR with peak energy values of 20, 60, and 80eV by measuring Si2P peaks in the XPS. On the other hand, after irradiating UR with peak energy values of 100 and 120eV, Si-Si bonds were not generated as shown in Fig.1. It may suggest that the Si-Si bonds generations are influenced by the  $L_3$  absorption at 99.2eV for Si. The modified layer was very shallow, because the generated Si-Si bonds on the surface were disappeared after etching the sample up to a depth of 1.5 nm as shown in Fig.2. The etched sample in Fig.2 shows the same SiO<sub>2</sub> bond peak without a Si-Si bond peak as in the original ones. In GeO<sub>2</sub> doped SiO<sub>2</sub> films irradiated by UR, almost the same tendency were found for the Si-Si bonds generation. The depth profile was also the same as that in the Fig.2

As for the Ge3d peaks in  $GeO_2$  doped  $SiO_2$  films after irradiating UR, the reduction layer with Ge-Ge bonds was also found to be generated especially for



FIG.1. Si2p peaks in the XPS spectra, before and after irradiating UR with peak energy from 50 to 120 eV in pure  $SiO_2$  films. Si-Si bonds are generated for the sample for peak energies less than 100eV. The UR dose was 1000mAh.

low peal-energy such as 50 or 60 eV as shown in Fig.3. The Ge-Ge peak decreases gradually by increasing the peak energy of UR. For a sample irradiated with peak energy of 100 or 120eV, peaks for Ge-Ge bonds are not seen in Fig.3, but this might be caused by a weak intensity for the Ge3d peak as compared to that for Si2p. The threshold energy is not clear for the Ge-Ge bonds generation comparing to that for the Si-Si bonds, which may be caused by the absence of clear absorption-edge for Ge around the irradiation energy range. After etching the sample, the reduction layer with Ge-Ge bonds was removed by 40 nm-deep etching. The Ge-Ge bonds layer is generated deeper than that for the Si-Si bonds layer of 1.5nm, which may be a cause of a penetration-depth difference for the effective irradiation wavelength.

The surface reduction effects appeared in Fig.1 was changed by other samples with different film thickness. A sample with thinner film with the same irradiation condition showed more intense peaks for Si-Si bonds in the XPS. Sample temperature might be the origin for the thickness dependence, because the sample temperature might be more than a few hundreds of degrees during the irradiation.



FIG.3. Ge3d peaks in the XPS spectra, before and after irradiating UR with a peak energy from 50 to 120 eV in GeO<sub>2</sub> doped SiO<sub>2</sub> films. Ge-Ge bonds are generated for the sample for peak energies of 50 and 60eV. The peak intensity for the Ge-Ge bonds (Ge<sup>0</sup>) is gradually decreased for peak energy from 80 to 120 eV, The UR dose was 1000mAh.



FIG.2. Si2p peaks in the XPS spectra, before, after irradiating UR with a peak energy of 60 eV and after etching up to a depth of 1.5 nm in SiO<sub>2</sub> films. The generated Si-Si bonds are disappeared after the etching as in the non-irradiated sample. The UR dose was 1000mAh.



FIG.4. Ge3d peaks in the XPS spectra, before, after irradiating UR with a peak energy of 60 eV and after etching up to a depth of 40nm in GeO<sub>2</sub> doped SiO<sub>2</sub> films. The generated Ge<sup>0</sup> peaks are disappeared gradually by increasing the etching depth. After 40nm etching, Ge<sup>0</sup> and Ge<sup>4+</sup> peaks are almost the same as that in the non-irradiated one. The UR dose was 1000mAh.

## Conclusions

UR irradiation effects are investigated for an application of silica-based materials to optical waveguide devices. Although large refractive-index changes were obtained by SR and UR irradiation in silica-based films in our previous report<sup>1)</sup>, other modification effects such as the surface reduction shown here are also important in the applications as an utilization tool and an obstacle for other applications. In our results, it is shown that the surface modification effects for Si and Ge bonds could be controlled by changing the peak energy of UR. From those results, UR is expected to be a useful irradiation source for modifying materials effectively and also controlling the modification effects as a desired way.

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# Characterization BN Thin Film Deposited on Cemented Carbide using Soft X-ray Absorption Spectroscopy

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## Abstract

Crystalline structure of BN thin film deposited on cemented carbide substrate by magnetron sputtering technique was characterized using soft X-ray absorption spectroscopy (XAS). Boron and nitrogen K near edge X-ray absorption fine structures (NEXAFS) of the BN thin films were measured with total electron yield (TEY) method and total fluorescence yield (TFY) method. The film structure changed dramatically from t-BN phase to c-BN phase when film thickness increased from 6.5 nm to 20 nm. The crystalline structure of the film deposited on the WC substrate with a bias voltage of -90 V was still t-BN type. However, the structure changed to c-BN phase when the bias voltage increased to -130 V.

## Introduction

As similar to carbon allotropic forms, boron nitride presents a polymorphism of hexagonal structure (h-BN) having a hexagonal plane network; such as graphite, and cubic structure (c-BN) having a steric structure; such as diamond. It is well known that h-BN is a relatively soft material. However, c-BN is known to be the second hardest material after diamond. The preparation of c-BN thin film for a coating material onto cutting tools is extensively studied. In cases of BN thin film fabrication by sputtering or ion plating depositions, h-BN structure is preferentially formed because it is a stable phase at normal pressures. Stably-forming technology for c-BN structure thin film was not confirmed as affairs.

Characterization of crystalline structure of BN thin film is indispensable to confirm the fabrication technology. Near edge X-ray absorption fine structure (XANES) spectroscopy is an appropriate technique to identify the crystal structure of BN thin film because the spectra of c-BN and h-BN are quite distinct and the bonding state on  $sp^2$  and  $sp^3$  can be observed in isolation. In this study, NEXAFS measurement at B-K and N-K edge was carried out for the characterization of crystalline structure of BN thin film deposited on cemented carbide (WC) as well as Si wafer by an RF magnetron sputtering technique.

#### **Experiments**

BN thin films were prepared on Si (100) and WC substrates by the RF magnetron sputtering system. The substrate holder was electrically floated for applying a bias voltage and could be heated up to 600°C, simultaneously.  $Ar+N_2$  mixed gas was used as working gas, and its pressure was 0.4 Pa. The DC bias was changed from -80 to -130 V in this study. Atomic composition of the prepared sample was determined by an Auger electron spectroscopy (AES).

B-K and N-K NEXAFS spectra of prepared samples were measured in the analyzing station of the beamline BL9a at the NewSUBARU SR facility. The beamline monochromator was mounted with a plane varied-space grating with central groove density of 1200 l/mm, the energy resolution of which was about 0.2 eV near the photon energy of 400 eV. The measurement was conducted with a total electron yield (TEY) method with sample current mode and with a total fluorescence yield (TFY) method with measuring the amount of fluorescence by a photodiode [1] for the same sample at the same position. It is well known that the TEY method can yield information in a shallow region from the sample surface because of the small escape length of photo-generated electrons of less than about 5nm [1, 2]. Meanwhile, the TFY method can yield information in a deeper region (bulk) of the sample of more than 100 nm [1] because of the much longer penetration depth of soft X-ray photons.

## **Results and discussion**

In order to clarify the growth process of BN films containing the c-BN phase, the films were deposited for 1, 2, 3, 5, and 30 min at 600°C and applied bias voltage of -90 V. Figures 1 and 2 show the B-K and N-K absorption spectra of a prepared films, respectively. The thicknesses of those films were estimated to 6.5, 13, 20, 33, and 200 nm using the deposition rate. For the 6.5-nm-thick film, both B-K edge and N-K edge spectra have a large  $\pi^*$  resonance peaks at 192 eV for B-K and at 401 eV for N-K edges, respectively, which are caused from sp<sup>2</sup> bonding states like a graphite. As the thickness increases to 20 nm, the  $\pi^*$  peak at 401 eV in N-K edge spectra becomes a shoulder. The B-K edge spectrum for the 20-nm-thick film also shows that film has an c-BN-dominant strucrure in spite of the presence of the small  $\pi^*$  peak. The NEXAFS spectra for the films with the thicknesses of 33 nm and above are almost the same as the spectraum of the 20-nm-thick film. This means that the t-BN (or h-BN with sp<sup>2</sup> bonding) underlayer thickness of the film deposited at 600°C was less than 20

nm and that the c-BN-dominant layer grew from an early stage of the deposition. It was also found from the measurement of incident angle dependency that the t-BN underlayer had a preferential orientation of the c-axis parallel to the film surface. The results also correspond well to the results of infrared absorption spectra measured with FT-IR spectrometer [3].





Fig. 1 B-K NEXAFS spectra of BN thin films with various film thicknesses prepared on Si wafer at 600°C.

Fig. 2 N-K XANES spectra of BN thin films with various film thicknesses prepared on Si wafer at 600°C.

After the structural investigation on the Si substrate, we deposited BN films onto the Si wafer and the cemented carbide (WC) substrates at the same time with substrate temperature of 600°C. At the negative bias voltage of -90 V, the crystalline structure of the film deposited on the WC substrate was still t-BN phase as shown in Fig. 3, though the structure of film simultaneously deposited on the Si wafer was c-BN phase. N-K NEXAFS spectra at different angles of incidence of 90° and 45° for the prepared BN film are shown in Fig. 3 for TEY and TFY methods. Although, the  $\pi^*$  resonance peak measured by TFY method (bulk) shows a small dependency of incident angle, the angular dependency is very large for the spectra obtained by TEY method (srrface). When the negative bias voltage increased to -130 V, the NEXAFS spectrum on WC substrate changed dramatically to c-BN phase as shown in Fig. 4.

It is difficult to evaluate the crystalline structure of BN film deposited on WC substrate by transmission type FT-IR spectroscopy. Therefore, the results obtained in this study suggests the effectiveness of X-ray absorption (NEXAFS) spectroscopy for evaluation of crystalline structure of BN thin films deposited on WC substrates.



Fig. 3 N-K NEXAFSS spectra of the BN thin film prepared on WC substrate with a bias voltage of -90 V.



Fig. 4 N-K NEXAFS spectra of the BN thin film prepared on WC substrate with a bias voltage of -130 V.

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# Spectral Recovery of Etching Damage by Soft X-ray Irradiation Observed in XAS spectra of TiO<sub>2</sub> Thin Film

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#### Abstract

We analyzed  $TiO_2$  thin films etched with capacitively coupled plasma etching apparatus by near edge X-ray absorption fine structure (NEXAFS) method. As a result, spectral change due to disordering of the crystalline structure was observed by TFY method in the sample treated with higher gas pressure. We also found that Ti-L spectra of etched sample was recovered to as-grown like by irradiation with soft X-rays (496 eV) for 10 min. This recovery occurred not only on the irradiation point of soft X-rays but also on the point 2 mm or more away. Furthermore, it was found that the spectral recovery can also be observed for the surface irradiated with ultraviolet (UV) light instead of soft X-rays.

#### Introduction

 $TiO_2$  is expected to apply as MOS gate oxide film because of its high dielectric constant. To use  $TiO_2$  as MOS gate film, it has to be processed by etching. However, there are few reports about the effect of etching damage to  $TiO_2$  thin films by etching process. Therefore, we analyzed the effect of etching damage to  $TiO_2$  samples by NEXAFS method. As it happens, we found the phenomenon in the analyzing process that disordered NEXAFS spectra of the etched film recovered to as-grown like by irradiation with soft X-rays.

The purpose of this study is the elucidation of the phenomenon that NEXAFS spectra of etched  $TiO_2$  thin film were recovered by soft X-ray irradiation. We investigated the condition of the etching damage to recover. For example, recovery of the spectra is studied for irradiation condition, light source, and irradiation position.

## Experiments

TiO<sub>2</sub> thin films were deposited on a glass substrate (Corning 1737) by facing cathodes DC magnetron sputtering system. We used capacitively coupled plasma (CCP) etching apparatus (Tokushima Univ.) to etch the samples. The etching gas was N<sub>2</sub> and its pressure and etching time were varied from 10 to 100 mTorr and 5 to 200 minutes, respectively. These samples were analyzed by NEXAFS method conducted at BL09A in the NewSUBARU synchrotron radiation facility<sup>[1]</sup>. The measurements were carried out with total fluorescence yield (TFY) method (bulk sensitive) and total electron yield (TEY) method (surface sensitive) at the Ti-L<sub>2,3</sub> edges (443 ~ 496 eV)<sup>[2]</sup>. NEXAFS method can obtain the information of chemical state or local structure around the element selectively by measuring an absorption edge of any element in the sample in non-destructive.

#### Results

As shown in Fig.1 (a), the spectra measured by TFY method was changed that the peak near 467 eV became lower with increasing the etching gas pressure. However, as shown in Fig.1 (b), there was little change due to increase of the gas pressure in the spectra by TEY method. Therefore, we got a very strange result that the etching damage of the sample surface was small but the damage at the sample inside was larger.

Continuing the measurement in order to investigate the cause, we found that the spectra of the etched sample were recovered to as-grown like by soft X-ray irradiation. Fig.2 shows the recovery process of the NEXAFS spectra by soft X-ray irradiation measured with TFY method. The etching gas pressure of the sample was 100 mTorr, and the etching time was 60 minutes. The spectrum of etched sample became as-grown like by soft X-ray irradiation (496 eV, tens of mW/cm<sup>2</sup>) for 30 minutes. After the irradiation, the spectra of recovered samples were returned to disordered shape by exposure to air, and then measured again after 21 days later. After returning to disordered shape by air exposure, the sample spectrum changed to as-grown like again by re-irradiation with soft X-rays for 10 minutes.

The bonding orbital around the Ti atoms should be disturbed by generation of oxygen vacancies. The spectra should be disturbed by disarray of crystalline structure. Therefore, it was considered that the spectra were recovered by supplement of the defective part. Since the spectral recovery by soft X-ray irradiation returned to that of after etching by exposure to the air, we considered that the spectrum recovered apparently by electrons which are from the electron-hole pairs generated by light irradiation and are trapped at the oxygen vacancies.

Etched Sample was irradiated with soft X-rays for 25 minutes at the center position of the sample in order to find out whether NEXAFS spectrum was recovered as spatially distributed. After irradiation, the sample was measured at the position separated from 2 mm above and below the irradiation center. soft X-rays were not irradiated at the position separated 2 mm from the center because the beam size of irradiated soft X-rays in

BL09A is 0.8 mmH  $\times$  0.3 mmV. However, the spectrum was recovered as-grown like not only at the center position of the sample but also the position separated 2 mm above and below from the center. We consider that recovery of spectrum was observed at the position outside of the irradiation due to the diffusion of generated excitons to the periphery of the irradiation position as free excitons.

If the fact of spectral recovery is caused by excitons generated by soft X-ray irradiation, it is considered that the spectra should be recovered by UV irradiation instead of the soft X-rays, the energy of which is above the band gap energy of anatase  $TiO_2$  (3.2 eV). Therefore, we tried to irradiate UV light (3.4 eV, 49 mW/cm<sup>2</sup>) to the etched sample (CCP-N<sub>2</sub>, 100 mTorr, 60 min) in vacuum. Fig.3 shows the recovery process of the NEXAFS spectra by UV irradiation. From the results above, it was considered that the spectral recovery of the etched sample should be apparent recovery due to the electrons generated by soft X-ray irradiation and trapped in the oxygen vacancies.



Fig.1 Ti-L<sub>2,3</sub> NEXAFS spectra of etched TiO<sub>2</sub> thin films (a): TFY method and (b): TEY method.



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# Modification of Electronic States of Multi-layer Graphenes by Ion Irradiation

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## Abstract

Low energy Ar ions (0.5 - 2 keV) were irradiated to multi-layer graphene films and the local electronic states were investigated by x-ray absorption spectroscopy (XAS). XAS analysis indicated that the number of sp<sup>2</sup>-hybridized carbon (sp<sup>2</sup>-C) atoms decreased after ion irradiation. At the same time, sp<sup>3</sup>-hybridized carbon (sp<sup>3</sup>-C) atoms were suggested to be formed in the multi-layer graphenes.

## Introduction

Graphenes [1] have been attracting tremendous attention as new semiconductors because of their intriguing properties, such as the extraordinarily high room-temperature carrier mobility, high thermal conductivity and high Young's modulus. These properties of graphenes can be employed in numerous potential applications such as transparent conductors and quantum devices. On the other hand, the control of electrical and optical properties is essential to realize graphene devices. Irradiation of graphenes with energetic particles is thought to enable us to control their properties and structure [2,3]. It has been reported that the doping level of graphenes can be also controlled by ion irradiation [4]. Several analytical techniques can be used to characterize irradiated graphenes. For example, Raman spectroscopy [5-9], transmission electron microscopy (TEM) [10], scanning tunneling microscopy (STM) [11], and X-ray photoelectron spectroscopy (XPS) [3] have been employed to study the properties and structure of irradiated graphenes. Soft X-ray absorption spectroscopy (XAS), on the other hand, is a powerful tool since it provides information on not only the local electronic structure surrounding excited carbon atoms, but also the orientation of the carbon  $\pi$ bonds [12]. In this study, to modify the electronic states of the multi-layer graphenes by the irradiation, we irradiated multi-layer graphenes with low-energy Ar ions (0.5-2 keV), and investigated the local electronic states by XAS.

## **Experiments and Results**

Multi-layer graphene films were synthesized by thermal catalytic chemical vapor deposition. Figure 1(a) shows a transmission electron



Fig. 1. (a) Cross-sectional TEM image of as-prepared multi-layer graphene films. (b) 2D peak of Raman spectrum of as-prepared graphene films.

microscopy (TEM) image of as-prepared multi-layer graphene films. The number and the total thickness of graphene layers were 6 and about 2 nm, respectively. We employed a Kaufman ion source (ULVAC-PHI MOD 04-370B) to irradiate the multi-layer graphene films at room temperature (RT) with Ar ions. The incident energy ranged from 0.5 to 2 keV and the dose varied between  $1 \times 10^{13}$  and  $1 \times 10^{15}$  cm<sup>-2</sup>. Micro-Raman spectra were taken with Ar ion laser (514.5 nm) using a Raman spectroscope (JASCO, NRS-2100). Fig. 1(b) shows the 2D peak of the Raman spectrum of the graphene films. It has been reported that the 2D peak changes in shape, width, and position with increasing number of graphene layers [13]. On the basis of the previous assignment, the number of graphene layers is estimated to be 3–5. This result is consistent with the results of TEM. The carbon K-edge XAS measurement was performed using BL09 of the 1.5 GeV synchrotron radiation source NewSUBARU at the University of Hyogo [14]. The total electron yield method was used for the measurement.

In order to explore local electronic states of the multi-layer graphene films, XAS was utilized for the multi-layer graphene films irradiated under different conditions. The spectra were measured at different angles of incident soft X-rays to the substrate surface  $(\alpha)$  and normalized to their intensity at ~320 eV. Fig. 2 is the XAS spectra of graphene films irradiated at an energy of 1 keV, taken at  $\alpha$ =55°. The  $\pi^*$  peak of 285 eV and  $\sigma^*$ peak of 292 eV were clearly observed. The sp<sup>2</sup>-C atom generally exhibits both  $\pi^*$  and  $\sigma^*$  peaks, whereas the sp<sup>3</sup>-C atom exhibits only the  $\sigma^*$  peak [15]. It was found that the intensity of the peak decreased with increasing ion fluence. This indicates decreasing number of sp<sup>2</sup>-C atoms after the ion irradiation. At the same time, an additional shoulder at ~289 eV is also recognized after the ion irradiation, as shown by arrow in Fig. 2. The energy at the shoulder is close to that at the C-K absorption edge for single-crystal diamond, and may be related to the formation of sp<sup>3</sup>-C atoms in the multi-layer graphene films [16]. With increasing ion fluence, an additional peak at ~287 eV was recognized in the XAS spectra, as shown by arrow in the Fig. 2. Additional peaks at ~289 eV and ~287 eV, which appeared similarly in the previous study for the study for the damaging stages of multiwalled carbon nanotube films [17], have been respectively assigned to relate to the formation of sp<sup>3</sup>-C and dislocation dipoles. The dislocation dipoles possess fivefold and sevenfold rings, thereby inducing the buckling and the rotation of the hexagonal networks [18-20].



Fig. 2. XAS spectra of multi-layer graphene films irradiated by 1 keV Ar ions at different fluences.

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# Fabrication of amino acid analysis chip using SR direct dry etching of PTFE

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## Abstract

Polytetrafluoroethylene (PTFE) is very attractive material for various fields, because of its chemical resistance and heat resistance, etc. But, micro fabrication of PTFE is very difficult from its high stability. Therefore, PTFE has never been applied to micro fluidic device. However, it is known that synchrotron radiation (SR) induces scission of polymer chain of PTFE. We have ever been succeeded in the fabrication of PTFE micro fluidic chip using SR dry etching and thermal compression bonding. As a next step, we have been engaged in the fabrication of PTFE micro fluidic chip for amino acid derivatization process. PTFE is an ideal material for performing the derivatization process. Because, this process using some strong acid, and some processes such as extraction and hydrolysis require high temperature heating operation. There is no precedent of the application of such complex micro structure made of PTFE to the device for chemical analysis.

## Introduction

In Solar system bodies, Amino acids, which are biologically important organic compounds, have played a key role in the chemistry that led to the origin of life on Earth. Precise analysis of the amino acid contained in extraterrestrial samples is very important in the study of the origin of life. We recently have opportunities for analyzing fresh extraterrestrial samples by collection of cosmic dust and sample return from asteroids, etc [1]. However, the amounts of the samples which can be used for analysis are limited because the samples are small in amount. Therefore, amino acid analyses for the samples using a micro fluidic chip are required. In this study, we develop the micro fluidic chip which can realize fluorescent derivatization required for optical isomer ratio analysis of the amino acid included in the samples.

## **Experiments and Results**

The sequence of analysis operations for the amino acid in the extraterrestrial samples includes extraction, filtration, hydrolysis, and evaporative drying. Therefore, high chemical resistance and heat resistance are required for the material of the chip. For this reason, we chose polytetrafluoroethylene (PTFE) as a chip material. PTFE has very excellent chemical stability, and its heat resistance is far higher than those of plastic materials. Although the PTFE has the high chemical stability, micro fabrication of PTFE is difficult because the small modulus of elasticity is not suitable for normal mechanical processing. Up to now, micro fluidic device made of PTFE has never been reported. It is known that synchrotron radiation (SR) induces scission of polymer chain of PTFE [2 3]. Figure 1 shows the etching mechanism of SR direct dry etching of PTFE. We have been fabricated PTFE microstructures by direct dry etching using SR [4]. The combination of PTFE microstructure using SR dry etching process and compression bonding enables us to PTFE micro fluidic chemical analyzer. In previous study, we fabricated simple micro fluidic chip which had only one micro channel.

In this study, we developed a novel micro fluidic device which had multiple micro channels and incorporated a filter structure for filtration. Figure 2 shows the schematic diagram of fabricated amino acid analysis device. This device consists of two chips, and the function of valve is performed by sliding of the upper chip. The micro channels are incorporated into the lower chip. The lower chip has four reservoirs for reagent such as derivatization reagent, and each reservoir can hold 10µl. In addition, we disposed two reaction reservoirs for extraction and derivatization into the lower chip. Extraction reservoir has micro filter for filtration of protein contained in the sample on the downstream side of reservoir. We set the filter dimension to 50µm square because the size of extraterrestrial sample is assumed to be 100–200µm in diameter. Derivatization reservoir operates the hydrolysis of protein to amino acid and fluorescent derivatization. Heating operation in the derivatization reservoir using the slide mechanism. In addition, the filter structure is incorporated in the derivatization reservoir for prevention of liquid leakage. For the function of the capillary valve, we set the filter dimension to 50µm square.

There is no precedent of the application of such complex micro structure made of PTFE to the device for chemical analysis. This study is very important for progress of science, technology and space development because our device has the potential to perform the chemical analysis with laboratory level on the spot where we are difficult to visit.



Figure 1. Etching mechanism of SR direct dry etching of PTFE: (a) drastic bond break in near surface, (b) bond break deep inside of the substrate and vaporizing from surface, (c) melting point shift and vaporizing from deep inside of the substrate, (d) penetration of mask pattern.



Figure 2. Schematic diagram of amino acid analysis device.

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# Powder Transport Direction Control Method by Using Drive Frequency of Surface Acoustic Wave

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#### abstract

We propose a novel method for controlling the powder transport direction by drive frequency, and demonstrate the validity of this method by experiments. In our experiments we could observe several powder transports by specific combinations of inclination angles and drive frequencies.

## Introduction

To integrate a lab-on-a-chip has been extensively studied. The surface acoustic wave (SAW) is particularly interesting because of its ability to add a novel liquid actuation method which makes to simplify the designing of lab-on-a-chips. Up to now, we succeeded in developing (SAW) actuators for transporting continuous liquid and a high-efficiency liquid mixing chip using SAW actuators [1]. Meanwhile, the displacement of solid by the SAWs had been reported [2]. If powder can be transported, we can establish a ontrolling process consisting of powder movement, powder injection into liquid, and themselves mixing operated only by the SAWs on one-chip. However, unlike continuously flowing liquid in a channel, spatially controlling powder transport by using the SAWs is difficult, because the powder transport direction must be aligned with an axis direction of an interdigital transducer (IDT) that generates the SAWs. Therefore, we changed the method for controlling the powder transport direction by using reflected SAWs from a micro groove and succeeded in moving the powder by the reflected SAW [3]. Moreover, if the powder can be transported in not only the upstream direction but also downstream direction of the SAWs, the flexibility of powder transport direction by drive frequency, and demonstrate the validity of this method by experiments.

Figure 1(a) shows a photograph of our fabricated SAW actuator for powder transport. The SAW actuator was fabricated by IDT (1- $\mu$ m thick Al layer) patterning on a piezoelectric substrate (127.8 degree y-rotated x-propagating LiNbO<sub>3</sub>) using photolithography. We fabricated four SAW actuators on a 4-inch wafer. Figure 1(b) shows a schematic diagram shown relationship between IDT and orientation flat of the wafer. The IDTs of the SAW actuators were located at inclination angles  $\theta$  of 0, 30, 60, and 90-deg. against perpendicular direction of the wafer orientation flat. Here, we chose a proven IDT shape of a 200 $\mu$ m stripline pitch, a 5mm aperture, and 20 stripline pairs.

## **Experiments and Results**

Figure 1(a) shows a photograph of our fabricated SAW actuator for powder transport. The SAW actuator was fabricated by IDT (1- $\mu$ m thick Al layer) patterning on a piezoelectric substrate (127.8 degree y-rotated x-propagating LiNbO<sub>3</sub>) using photolithography. We fabricated four SAW actuators on a 4-inch wafer. Figure 1(b) shows a schematic diagram shown relationship between IDT and orientation flat of the wafer. The IDTs of the SAW actuators were located at inclination angles  $\theta$  of 0, 30, 60, and 90-deg. against perpendicular direction of the wafer orientation flat. Here, we chose a proven IDT shape of a 200 $\mu$ m stripline pitch, a 5mm aperture, and 20 stripline pairs.

Figure 2 shows frequency characteristic of return loss (RL) of our fabricated SAW actuator. The RL is the logarithmic ratio of the incident electric power PI to the reflected electric power PR and increases as the applied power ratio to the IDT increases. At the SAW actuator with 0-deg. inclination angle, one RL peak was observed at 19.1MHz, and then multiple peaks were observed. The 19.1MHz is the conventional drive frequency of the SAW actuator, and corresponds approximately to the value of propagation velocity of a Rayleigh-wave (3690m/s) divided by IDT's pitch size (200 $\mu$ m). On the other hand, because there existed the multiple peaks, it is considered that the SAW actuator had potential to generate SAWs at their peak frequencies. In the same way as the SAW actuator with 0-deg inclination angle, there exist lots of RL peaks in the other SAW actuators with

different inclination angles.

Next, we investigated powder transport behaviors by the SAW actuators applied at the RL peak frequencies as drive frequencies. Figure 3 shows experimental setup for powder transport. Before starting the experiments, the powder was uniformly spread on the wafer by a sifter. Here, for the powder we used tungstic anhydride (average particle size of  $22.3 \mu$ m) in consideration of visibility and insulation. In the experiment, a function generator created 1-kHz burst waveforms consisting of 2000 cycles of f<sub>D</sub> MHz sine waves, where, it, corresponded to the obtained RL peak frequencies. If SAWs were generated by applying the boosted voltage, the powder might be transported by the propagated SAWs. At this time, the powder transport behavior was recorded with a high-definition video camera.

In our experiments we could observe several powder transports by specific combinations of inclination angles and drive frequencies. The most notable ones are that the SAW actuator with 90-deg. inclination angle could transport the powder forward and backward with high transport efficiencies in comparison with the other SAW actuators. The investigation powder transport characteristics with different inclination angles can be very useful in the designomg a chip consisting of the SAW actuators for powder transport control







Figure 2 Frequency characteristic of return loss of SAW actuator.



Figure 3 Experimental setup for observing the powder transport driven by SAW actuators.

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# Fabrication of SERS Active Three-dimensional Silver Nanostructure

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## Introduction

Recently, surface enhanced Raman scattering (SERS) is attracting attention as a high sensitive analysis system. SERS is the detection method using Raman spectroscopy and localized surface plasmon resonance (LSPR). To enabling strong LSPR, the noble metal nanostructure like gold or silver is essential. In previous report, gold nanoparticles were used to fabricate nanostructure. In this study, by using convective self-assembly [1] of particles, we developed the three-dimensional silver nanostructure (Ag3D) because low cost silver is more desirable material for SERS active nanostructure than gold. In addition, silver is thought to be suitable for the SERS measurement of various compounds.

## Fabrication of Ag3D

We pasted silicone sheet with 6 mm throughhole on the UV-cleaned slide glass, and made a well. 5µl of the mixed solution of the silver nanoparticle (AgNP) and polystyrene latex beads (PS) was dropped into the well and dried at 75 % relative humidity for about 1 day. The PS colloidal crystal was fabricated by convective self-assembly, where AgNP were simultaneously accumulated in the gaps of the PS. The structure was soaked in dichloromethane to remove PS. Thus, Ag3D was successfully obtained (Fig.1).

#### **SERS** measurements

As shown in Fig.2, unique honey-comb structure of Ag3D was fabricated at a part of the well. We demonstrated in situ SERS measurement of 4,4'-Bipyridine (4bpy) as the Raman active molecule, using the Ag3D. First, silicone sheet with 6mm throughhole was pasted to the Ag3D on the glass to make a measurement well. Second, 35  $\mu$ l of 4bpy aqueous solution was dropped into a well on the Ag3D. A cover glass was put on to prevent drying of 4bpy solution and changing of 4bpy concentration. Ag3D was set to Raman spectrometer, and 1 s irradiation of 785 nm (50 mW) laser focused on the Ag3D was started.

We observed the characteristic enhanced Raman spectrum of 4bpy (1000 cm<sup>-1</sup>, 1250 cm<sup>-1</sup>, 1580 cm<sup>-1</sup>) within 1 min after dropping 4bpy (Fig.3). SERS spectrum was only observed in the part of Ag3D, while no SERS was observed in the part without Ag3D. Raman spectra were enhanced about 10<sup>5</sup> times, compared with the case without Ag3D. Although the peak of 1 nM 4bpy solution was weak, it was detectable. The case with Ag3D and the case with Ag colloid aggregation were compared in the 4bpy peak height of 1580 cm<sup>-1</sup> (Fig.4). SERS measurement using Ag3D was stable even after time passed, while peak intensity drastically dropped within minutes in the case with Ag colloid. one reason for this was that SERS active structure of Ag colloid was broken by aggregation process over time. In addition, we succeeded in observing the chloride activation which increased to 2-3 times in Raman intensity of 4bpy by the addition of NaCl to Ag3D (Fig.5). As a result, we have achieved a high sensitivity SERS measurement using Ag3D. SERS activity of Ag was generally higher than Au in the colloidal system, although obtained SERS using Ag3D [2] was still weak compared to the case using Au3D which was consisted gold nanoparticles. There is a possibility of enabling strong SERS if Ag3D fabrication is optimized.



Fig.1: (a) A schematic diagram of self-assembled structure. (b) Ag3D after drying and remove PS



Fig.2: Microscopic image of three-dimensional silver nanostructure.



Fig.3: SERS spectra of 4,4'-Bipyridine.

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Fig.4: 4,4'-Bipyridine peak intensity with Ag3D and Ag colloid aggregation.



Fig.5: Chloride activation of 4,4'-Bipyridine

# **Blood separation chip**

# for automated biological analysis

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Abstract

We present a chip for the blood separation using centrifugal force and capillary force. We expect that this chip can perfome overall assay with high-efficiency and significantly shorten the analysis time by integrate our proposed 3D lab-on-a-CD. The material of the chip which is fabricated by using X-ray lithography is SU-8 and Si. Blood separation is done using centrifugal force by spinning the chip at a frequency of 40Hz and transport to collection reservoir from separation reservoir using capillary force. It is necessary for capillary force to treat surface condition. We succeed in liquid transportation by only control spin speed.

#### Introduction

The lab-on-a-CD is promising for the automation of multiple microreactor systems. Recently, high-performance immunoassay based on lab-on-a-CD has been proposed [1]. The extraction of plasma from whole blood is the first preparative step in many assay protocols and major importance in medical diagnosis [2]. We present a chip for the extraction of blood plasma from whole blood using centrifugal force of spin and capillary force. We expect that this chip can be overall assay with high-efficiency and significantly shorten the analysis time by integrate our proposed 3D lab-on-a-CD [3].

We present a chip for the blood separation using centrifugal force and capillary force. We expect that this chip can perfome overall assay with high-efficiency and significantly shorten the analysis time by integrate our proposed 3D lab-on-a-CD. The material of the chip which is fabricated by using X-ray lithography is SU-8 and Si. Blood separation is done using centrifugal force by spinning the chip at a frequency of 40Hz and transport to collection chamber from separation chamber using capillary force. It is necessary for capillary force to treat surface condition. We succeed in liquid transportation by only control spin speed.

## **Experiments and Results**

We designed chip as shown in Fig.1. We formed a  $CHF_3$  plasma chemical vapor deposition (CVD) film on the capillary valve just before the experiment. The plasma chemical vapor deposition (CVD) film with fluorine has a contact angle of over 100° [4]. By coating valve, liquid can be held until the higher rotation.

Process of blood separation is described in Fig.2. First of all, we injected whole blood into the separation reservoir (Fig.2a). In spinning the chip blood separation was performed by centrifugal force(Fig.2b,e<sup>(1)</sup>). Rotational speed is accelerated up to frequency of 25Hz(Fig.2e<sup>(2)</sup>). It was less than the burst frequency of the capillary valve. Phase separation was caused in a centrifugal field by a difference in mass density (Fig.2c). During blood separation, the capillary valve is used to control the flow sequence and hold liquid by surface tension. After finishing the separation, rotating speed was accelerated above the burst frequency. Then, the capillary valve was burst by the stronger centrifugal force (Fig.2d,e<sup>(3)</sup>). Next, liquid transportation was started and rotating speed should be decelerated to avoid disturbing rise by centrifugal force(Fig.2e<sup>(4)</sup>). Liquid rose in the capillary to the same height as the surface of liquid in the separation reservoir and reached the hydrophilic area, liquid is extracted by capillary force toward the collection reservoir. When liquid passed through the top of the capillary, rotating speed was accelerated again and extraction to the collection reservoir quickly(Fig.2e<sup>(5)</sup>). Blood cells remained at the bottom of the separation reservoir.

In this way, it is possible to control the flow sequence only controlling the rotation speed of the chip. We expect that the proposed chip will be able to extract only plasma from whole blood automatically.



Fig.1: Schematic of microchannel.



Fig.2: (a)-(d) Optical micrograph of each process of blood separation. (e)Protocol diagram.

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# **Optimization of Surface Enhanced Raman Scattering Active Three- Dimensional Gold Nanostructure**

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**Abstract:** Recently, Surface Enhanced Raman Scattering (SERS) attracts attention as a high sensitive analysis system. Taking into account that one dimensional linearly connected gold nanoparticles (AuNP) [1] and two dimensional array of elongated AuNP [2] showed longitudinal localized plasmon resonance and excellent SERS performance, three dimensional layer stacks of chain-like assembles of AuNP with numerous particle junctions are desirable. To accomplish thick stacks, we have focused on the three dimensional gold nanostructure (Au3D) using a casting method of convective self-assembly (CSA) of AuNP and polystyrene latex beads (PS) [3]. In this report, Au3D with thicker stacks was developed by optimization of AuNP and PS component in CSA and SERS measurements were demonstrated.

**Fabrication of Au3D and SERS measurement:** A PDMS sheet with a 6 mm through hole was attached on the uv-cleaned slide glass, where hydrophobic PDMS wall of the 6 mm well was made a circumference of "coffee-ring" so as to pin a drop of the AuNP ( $8.4 \times 10^{14}$  particles/l) and PSL ( $2.3 \times 10^{16}$ particles/l) mix dispersion with various composition which were dropped into the well. Since the hydrophobic surface of PDMS also made a convex meniscus of the drop around which surface/volume ratio was larger than other part of the drop, evaporation of water was accelerated around the circumference. As a result, the thickly stacked self-assembles on the edge of "coffee-ring" was formed. After soaking with dichloromethane to remove PSL, sterically-bulky Au3D with enough thickness was obtained as shown in Fig. 1.

In situ SERS measurement was performed using Au3D and 4,4'-bipyridine (4bpy) as the Raman active molecule. 4bpy aqueous solution (30  $\mu$ l) was dropped into the measurement well, and covered with a cover glass in order to prevent drying or concentration. The collection time of each SERS measurement was 1 second (average 10 times at 0.1 second) using Raman spectrometer (RAM-100S, Lambda Vision Inc., Yokohama Japan) with 785 nm laser (100 mW). As results, we succeeded in 100 nM 4bpy detection.

**Optimization of Au3D:** In order to obtain further SERS active structure, we performed optimization of Au3D fabrication concerning dropping volume of mixed dispersion (3, 5, 7, 10, 15, 20  $\mu$ l), the particle number ratio (AuNP:PS = 100:1, 300:1, 1000:1, 3000:1), Au diameter (16, 22 nm) and PS diameter (100, 600, 1400 nm). SERS active of the Au3D were evaluated by measuring 4bpy. As results, optimum conditions of dropping volume, the number ratio, Au diameter and PS diameter respectively were 5  $\mu$ l, 1000:1, 16 nm and 600 nm as shown in Fig. 2-4. By using Au3D of optimum conditions, we achieved high sensitive measurement of 1 nM 4bpy as shown in Fig. 5. This enhancement reached over 10<sup>7</sup> compared with the normal Raman spectroscopy without Au3D.

In addition, we found that Au3D's width in radial direction depended on Au particle number. Then, the width of Au3D was controlled as shown in Fig. 6. By using this broad Au3D, the background from the slide glass was reduced even inexpensive Raman spectrometer without confocal system. Further high sensitive detection is expected by using broad Au3D. Furthermore, we also succeeded in the detection of 10  $\mu$ M histamine and 50  $\mu$ M melamine. Au3D is to be applied to the field of bioassay and food safety.



Fig. 1. (a) SEM image of Au3D. The diameter of the holes is about 600 nm. (b) Enlarged SEM image of honeycomb network of granular assembled gold nanoparticles.



Fig. 2. Optimization of Au3D for SERS activity. Effect of particle number ratio (AuNP:PS).



Fig. 3. Optimization of Au3D for SERS activity. Effect of Au diameter.



Fig. 4. Optimization of Au3D for SERS activity. Effect of PS diameter.



Fig. 5. Characteristic enhanced Raman spectra of 4bpy with different concentration (100 nM, 10 nM, 1 nM, Blank) by using optimum Au3D.



Fig. 6. Changes in Au3D width in radial direction depending on the particle number. (a)  $0.5 \times 8.4 \times 10^{14}$  particles/I (b)  $8.4 \times 10^{14}$  particles/I (c)  $2.5 \times 8.4 \times 10^{14}$  particles/I (d)  $5 \times 8.4 \times 10^{14}$  particles/I.

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# Fabrication and characterization of three-dimensional type micro magneto-impedance sensor

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## Abstract

Fabrication and evaluation of a three-dimensional micro-scale magneto-impedance (MI) sensor have been carried out. We present the detail of the fabrication process of the device and the measurement result of the impedance of the sensor head. The measured characteristics indicate that we succeeded the fabrication of the three-dimensional micro-scale MI sensor.

## Introduction

In recent years, the people's concern about their health is increasing under the influence of aging society in advanced nations. Physical changes caused by external factor will be offset by the action of the autonomic nerve system. This indicates that the human health state depends on the autonomic nervous system. An un-invasive healthy monitoring system is required for the estimation and control of each of health status. The system consists of near-infrared spectroscopic devices for detecting the amount of substance inside blood and integrated magnetometric sensors to measure the dynamic characteristics of human's circulatory organ system as one of the function of the autonomic nervous system at the same time. The circulatory system response from the measurement results enable us to create the mathematical model which relates the response with exogenous stimulus. Therefore, health-maintenance medicine will be achieved by this model applied to the signal obtained from the sensor.

We need the high sensitive sensor in order to achieve the model. The change in the high frequency impedance of very soft ferromagnetic materials upon the action of external static fields, known as magneto-impedance (MI) effect, has been intensively studied for magnetic sensor applications.[1, 2] The high sensitive MI effect occurs when high frequency current is applied to the amorphous metal in which spin is arranged circumferentially. The MI sensors using MI effect has been recently attracting attention for improved the resolution of up to  $10^{-12}$  T [1], which can measure bio-magnetic field in range from  $10^{-10}$  to  $10^{-15}$  T. The significant change in impedance is basically derived from the skin effect. The estimation of the high sensitivity of magnetic field is of great importance for the sensor application. The development of the general estimation method for the only inductance component of impedance also provides an insight to understanding the physical mechanism with respect to the relationship between the skin effect and micro- or nano-scale magnetization structure.

## **Experiments and Results**

In this study, integrated coil, made of gold Au, is fabricated using UV lithography and succeeding packaging method to improve productivity. The  $Fe_{21.5}Ni_{78.5}$  (Permalloy: Py) wire with thickness of 60 nm is prepared in the coil. The devices were fabricated by building up SU-8 layers as shown in Fig. 1. The fabrication process is also schematically illustrated in Fig. 1. Finally, one side of the device is covered with Kapton film for electrical insulation. Its size is 1.5 mm in length, 1 mm in width, and the thickness is 35  $\mu$ m. The optical image of the device is shown in Fig. 2. In our device, the inductance component of impedance can be detected by not only the Py wire itself but also a pickup coil formed around the Py wire.

To evaluate the impedance of the device, we measured the impedance of the device as a function of the frequency (from 100 Hz to 100 MHz) by using a MI sensor electrical circuit device. As shown in Fig. 3, the impedance was rapidly increased with a frequency up to a 10 % when the frequency exceeded at about 20 MHz. The change in the impedance is attributable to not the ferromagnetic resonance but the normal skin effect because the ferromagnetic resonance frequency is far higher than the measured frequency region.

Although further systematic investigation is necessary in order to perfectly understand the physical mechanism and evaluate the MI effect, we have succeeded in fabricating a novel integrated MI sensor by means of UV lithography fabrication technique. The implementation of high sensitive MI sensors can provide biomedical monitoring system, car sensors and so on.



Fig. 1 Schematic of fabrication process and device.



Fig. 2 Optical images of (a) the fabricated MI Sensor and (b) magnified coil region.



Fig. 3 The frequency dependence of the impedance of the fabricated MI sensor.

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# Micro-Mirror Array Device for floating image manufactured by Synchrotron radiation

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## Abstract

We propose a new imaging optics called the Dihedral Corner Reflector Array (DCRA) which is designed to make the floating image. DCRA consists of numerous micro-mirrors placed perpendicular to the surface of substrate. The micro-mirror array is implemented by the inner walls of minute square holes or the side of minute square pillar. We can choose two types of the structure. The primordial is based on two reflections by a pair of adjacent mutually perpendicular mirrors, *i.e.*, a dihedral corner reflector. (S.Maekawa 2006.) Although the principal of operation is based on reflection by mirrors, the device is also transmissive and deflects light. Primordial of DCRA is not so complicated. However, it is too difficult to fabricate the DCRA by usual machining because of high aspect ratio micromachining. Therefore, in this manuscript, we fabricated the device by deep X-ray lithography due to synchrotron radiation. The characteristics of the fabricated DCRA are evaluated by the optical transmission and reflection measurements.

## Introduction

There are some basic imaging optics which can form a real image, such as convex lens, a concave mirror, and diffraction optics (a Fresnel lens). For example, there are systems which are based on the lens array of the Graded Index Lens (GRIN) (H.Kita et al 1971), Roof Mirror Lens Array (RMLA) (M.Kawazu et al 1985), and the stacking of various micro-lens arrays (R.Volkel et al 1996). These have an optical axis and a specific focal length. Moving an object closer to the optics, the real image forms farther from it and is magnified. In contrast, imaging optics can form three-dimensional (3D) images without distortion. An example of this is a plane mirror. However, as a plane mirror can only form virtual images, the world in the mirror is treated as fantasy.

The authors of this paper propose a new imaging optics forming a real mirror image with the use of micro-mirrors. We called this imaging optics as the Dihedral Corner Reflector Array (DCRA).



Figure 1 Operation mode of (a) two-dimensional- and (b) three-dimensional-dihedral corner reflectors.

## The primordial of DCRA

The primordial of DCRA is based on mirror reflection. Figure 1 describes the operation of dihedral corner reflector. The reflection mode of DCRA is limited, because incident light is reflected twice when passing through a dihedral corner reflector. In the case of two-dimension structure, an incident light from a light source "A" is reflected in the direction "B" parallel to the light source "A" as shown in Fig. 1(a). Next, let us consider that the incident light from "A" into a dihedral corner reflector reflects two times at the mirrors and deflects toward the point "B" in 3D structure as shown in Fig. 1(b). Then, if the micro-mirrors are extremely small, the incident light passes through the substrate plane toward the symmetric point for the light source. When we prepare many dihedral corner reflectors on the substrate, all the light from a light source is converged onto the reflection-symmetric point of the source. As a result, the array of numerous dihedral corner reflectors, namely DCRA, can realize the floating image. (S.Maekawa 2006)

## Image-formation and precision of DCRA

Here, we postulate that the transmittance of DCRA is the percentage of incident light through the reflection-symmetric point. The transmittance is given by

## Transmittance = $I \times R^2 \times T$ , (1)

where I is the ideal transmittance, R is reflectance of micro-mirror, and T is the losses, which is defined as the attenuation of intensity of the incident light after passing through the DCRA.

Reflectance of micro-mirrors is the most important factor in imaging by DCRA. In this study, we expect that it is as close as possible to 100%. However, in the device, the micro-mirrors placed perpendicular to the surface of substrate. Therefore, no one can be polished after manufactured. Accordingly, reflectance of micro-mirrors is determined during the creation of the DCRA.

The perpendicularity of dihedral corner reflector plays an important role on the resolution of the imaging, and it causes the distortion of the image. The dependence of the perpendicularity of the wall of DCRA can be estimated by using the simulation. This simulation enables us to calculate that the ray trace through position of light reflected by a line of plane mirrors from point light. Then, we can choose the value of the number of the plane mirrors, the distance of point light to the head mirror and the taper of mirrors. If the planes of mirrors in the DCRA are exactly perpendicular, all the reflected light by each mirror. The floating image produced by the DCRA can be estimated to be distorted up to 10  $\mu$ m when the plane mirrors have 1 minute taper.

Image resolution is determined by the dimension of the dihedral corner reflector. The higher resolution image can be obtained, the smaller dihedral corner reflectors in the DCRA are fabricated. However, the image produced by the smaller DCRA will darken because the diffractive component of the light increases.



Figure 2 Schematic of the DCRA device designed in this study.

Table 1 Dimension of DCKA		
Length of square side [µm]	150	
Pillar height [µm]	300	
Pitch [um]	25	

Pitch [µm]	25
Ideal transmittance [%]	100
Aperture ratio [%]	64.9
Perpendicularity [deg]	90
Roughness [nm]	10

## **Fabrication of DCRA**

Polishing the micro-mirrors is easy if they are parallel to the device surface. However, because micro-mirrors are perpendicular to the device surface in the DCRA, it is impossible to polish them in pre- or post- processes. Therefore, the micro-fabrication of high precision is required for the fabrication of DCRA. In this manuscript, we fabricated the pillar patterned DCRA made of Poly-methyl methacrylate (PMMA) by using synchrotron radiation (SR). The fabrication process using the SR enables us to fabricate the DCRA structure within the limit of accuracy of about 1 nm. Figure 2 shows schematic of dimensions of our DCRA device. As shown in Fig. 2, a dihedral corner reflector is made by a pillar with square section.

The incident light through inside of pillars made of PMMA in pillar patterned DCRA. Considering the PMMA refractive index, we design the aspect ratio (height/width) of our device is two in order to achieve that the theoretical value of light transmittance of our device is expected to be 100%. The aperture ratio, namely the portion of the opening, is determined by the pitch between the reflectors. We estimate the effective fraction transmitted of our device is 64.9% considering the contribution of the aperture ratio. Expressed in another way, the brightness of the floating image is expected to be 64.9% with the respect to that of an object. The dimension and desired values of DCRA are summarized in Table.1.



Figure 3 Schematic of transmission-reflection ratio measurement system.  $\Theta$  is an angle between the perpendicular direction of the incident light axis and sample horizontal plane.  $\phi$  is an angle between the perpendicular direction of the light axis and detector.



Figure 4 Optical microscope image of (a) top view and (b) cross section of the pillars in our DCRA.

Length of square side [µm]	(x) 150.92
	(y) 151.42
Pitch [µm]	25.87
Pillar height [µm]	326.78
Perpendicularity[minute]	5.8

Table 2 Dimension of the fabricated DCRA

## **Results and discussion**

Up to now, the criteria and evaluation method for the properties such as the resolution and brightness of the image produced by the DCRA have not yet been established. In this study, we evaluate the characteristics of the fabricated DCRA by measuring the dimension, perpendicularity of the reflector, fractional transmitted and reflection. The attenuation of brightness and reflection ratio are measured by transmission-reflection ratio measurement system as shown in Fig.3.

Figures 4(a) and 4(b) show a typical optical microscope image of top view and cross section of the micro-pillars in the fabricated DCRA, respectively. The measured average dimensions of the DCRA are summarized in Table 2. The measured dimensions except the perpendicularity are almost in good agreement with the design dimensions. The perpendicularity of the fabricated pillars have about 6 minute taper. The evaluation using the simulation indicates the taper structure causes the distortion of 65  $\mu$ m with respect to the distance of light source. This distortion is serious for the observation of a floating image formed by DCRA.

Next, the attenuation of brightness is evaluated by the transmission-reflection ratio measurement system shown in Fig. 5. The measured fraction transmitted was about 40%, being in acceptable range of the design. As shown in Fig. 5, we can see a broad change from 400 nm to 600 nm in wavelength. The change corresponds to the absorption derived from the discoloration of PMMA by SR.

Finally, the reflection ratio was evaluated by using the same measurement system. Here, the coordinate system is defined as shown in Fig. 3. In order to evaluate the angle  $\phi$  dependence of the single reflection of the DCRA at 700 nm in wavelength, we fixed the DCRA at the angle  $\theta = 25^{\circ}$ . The measured angle  $\phi$  dependence of the reflection is shown in Fig. 6. As shown in Fig. 6, two reflection peaks are observed. The peak with the larger amplitude (at about  $\phi = 0^{\circ}$ ) corresponds to the refractive incident light. The other is the single reflection of the light by the DCRA. If the ideal DCRA was fabricated, we would obtain the single reflection peak at  $\phi = 50^{\circ}$  in this experimental setup. However, we

found the single reflection was extended in the  $\phi$  range between  $40^{\circ}$  and  $70^{\circ}$  because the reflected light was spread by the distortion due to the taper. The actual fraction transmitted is estimated to be 5.4% by substituting the measured value into Equation (1). This indicates that a dark floating image is formed by the fabricated DCRA. However, we succeeded in forming the floating image by the fabricated DCRA as shown in Fig. 7.

The improvement of fabrication process and evaluation of the DCRA will open the door to the novel imaging devices.



Figure 5 Absorption as a function of wavelength.



Figure 6 The angle  $\phi$  dependence of the fabricated DCRA.



Figure 7 A typical floating image is imaged by the fabricated DCRA.

## Conclusion

We proposed novel imaging optics with micro-dihedral corner reflector arrays (DCRA) which can form a reflection-symmetric image as a real image in the air. It was fabricated by synchrotron radiation. We evaluated the fraction transmitted and single reflection of the fabricated DCRA by the optical measurement system. Although the performance of the DCRA was not good, the fabricated DCRA enables us to observe a floating image. By comparing the simulation result with the experimental evaluation, we can understand what worsen the performance of the DCRA.

Our main work to improve imaging in the future is to increase transmittance and establish the quantitative measurement method of resolution and reflection ratio.

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# Broadband noise spectroscopy of a magnetic wire

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## Abstract

We measured broadband magnetic noise spectrum induced in a single layered  $Ni_{81}Fe_{19}$  nano-scale wire biased with a dc-current in a frequency range from 500 MHz to 8 GHz. The magnetic noise spectra are recorded as a function of external magnetic field and dc-current. Experimental measurement results and analytical calculations reveal that the noise generation is caused by the thermal magnetization fluctuation due to ambient temperature and Joule heating.

## Introduction

The spin dynamics in a nano-scale magnet with a confined structure has gained increasing attention over the last decades due to the scientific and technological interest. [1] To understand the mechanism of the spin dynamics from a microscopic perspective, the special instrumentality and measurement system, such as magneto-optic Kerr effect, Brillouin light scattering and ferromagnetic resonance, are required until now. [1] Several electrical measurements that are suitable for investigating the spin dynamics in nano-scale magnets and are extremely sensitive have been proposed recently. One of them is the homodyne detection of the resistance change induced by the spin-transfer torque and magnetic fields. The magnetic noise measurement of a nano-scale magnet, in particular for giant magnetoresistive (GMR) devices and tunneling magnetoresistive (TMR) devices, can be used as other tools. [2, 3] The GMR or TMR noise tests are nondestructive and can be applied to the read heads for the magnetic hard disk drive. For diagnostic testing, we interested in the noise induced by the spin-transfer torque, magnetic fields and thermal excitation. [2-4]

This paper reports our investigation of broadband noise spectroscopy in a single layered  $Ni_{81}Fe_{19}$  (Permmalloy: Py) wire.

## **Experiments and Results**

The soft-ferromagnetic Py nano-scale wire is fabricated onto a polished MgO (100) substrate by means of high-resolution electron beam lithography with a standard lift-off technique. The thickness, width and length of the prepared Py wire are 20 nm, 2.2  $\mu$ m and 100  $\mu$ m, respectively. The wire is placed between the center strip-line of the coplanar waveguide (CPW) comprising Au conductive strip with thickness of 100 nm. The optical micrograph image and schematic circuit diagram for broadband noise measurement are shown in Fig. 1.

Figure 2 shows the homodyne detection spectrum (black solid line) [5] and the lock-in detection noise spectrum (red solid line). It should be noted that the resonance frequency around 3.8 GHz of the magnetization fluctuation signal almost matches that of the homodyne detection spectrum, indicating that the origin of the noise signal induced by dc-current is the same as that of the homodyne detection signal. We also measured the magnetic field dependence of the broadband noise spectra. As a result, the resonance frequency correlates well with the ferromagnetic resonance frequency, and the amplitude of the noise signal at the resonance frequency decreases with increasing the static field.

These experimental results suggested that the measured noise signal is derived from the magnetization precession induced by the thermal fluctuation. The present experimental results are in good agreement with the analytical solutions. [2-4] We believe this study provides not only the important physics on the fundamental limitation in the possibility of the scale-down size but also the improvement in the read heads and in the radio-frequency devices.



Fig.1 Optical micrograph image of the Py wire and schematic diagram of the broadband noise measurement circuit.



Fig. 2 Homodyne signal spectrum and broadband noise spectrum in magnetic field of 100 G at  $\theta = 45^{\circ}$ .

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# Defect Characterization of an EUV Mask using a Coherent EUV Scatterometry Microscope

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## Abstract

On extreme-ultraviolet (EUV) masks, phase structures such as bumps or pits on the substrate or particles buried in the multilayers can form printable defects at EUV exposure tool. Property of these defects is required for mask repair by defect hiding and compensation methods using the absorber pattern. We have developed a coherent EUV scatterometry microscope (CSM) to observe EUV masks, which uses a simple lensless system to record a diffraction image from mask patterns. We introduce preliminary observation results for programmed phase defects. We evaluated the defect width and height from the diffraction images, and the detection limit of the CSM system that focused to the illumination onto the defect with a 100 nm diameter. The diffraction image recorded by the micro-CSM system provides raw defect data, which is essential for defect compensation.

## Introduction

In extreme-ultraviolet (EUV) lithography, defect-free mask production is one of the critical issues for high-volume manufacturing. A mask is a master pattern for a semiconductor device, and there must be no defects on this mask. In EUV lithography, the EUV mask is a reflective type mask, unlike the transparent-type mask used for conventional 193 nm lithography. The EUV mask is coated with a Mo/Si multilayer, and an absorber layer, in which patterns are printed to form a device pattern. However, phase structures such as bumps or pits on the substrate or particles in the multilayers can form printable defects. For example, a shallow structure of 1 nm on the surface of a mask substrate causes a large reflection phase shift of 53° at EUV wavelength. As a result, this buried defect is printable.<sup>1-6)</sup>

Buried defects can be detected efficiently at the mask blank stage of manufacture, which is just before the deposition of the absorber layer. The Selete and EIDEC groups have developed an actinic blank inspection (ABI) tool to detect phase defects.<sup>7-10)</sup> The ABI tool is a dark-field EUV microscope composed of а discharge-produced-plasma source and Schwarzschild optics, which collects scattered EUV light from buried defects to form a dark-field image on a charge-coupled-device (CCD) camera. Because the defect signal is integrated in a dark-field, the ABI tool has a good signal-to-noise (S/N) ratio for the detection of defects.

Current EUV masks do not satisfy defect density requirements.<sup>11,12)</sup> As a result, defect hiding and defect compensation methods have also been proposed,<sup>13,14)</sup> which work by modifying the

absorber pattern to compensate the aerial image. Detailed defect information, such as defect position on the mask, defect size, and phase distribution, is necessary for the compensation process. However, the ABI tool is specifically intended for defect detection, for which the magnification requirement is not high. The spatial resolution is determined by the CCD pixel size, where one pixel integrates the scattering signal from a 500 $\times$ 500 nm<sup>2</sup> region on the mask. It is thus difficult to use the ABI tool to characterize the phase defect information. In this study, we observed the phase defects using a coherent EUV scatterometry microscope (CSM), which is a lensless type of microscope.<sup>15-19)</sup> The CSM records the diffraction from the mask directly using a CCD camera. We discuss the requirements for a defect characterization tool based on the preliminary observation results for programmed defects. We also propose a micro-CSM system for defect characterization, which focuses the illumination onto the defect with a 100 nm diameter.

## Experiment

We observed the phase defects using the CSM system shown in Figs. 1 and 2. The CSM system was installed at the BL-3 beamline of the NewSUBARU synchrotron radiation facility,<sup>20)</sup> which uses a bending magnet as a light source. Two toroidal mirrors collimate the white light into the CSM system. Figures 1 and 2 show a photograph and a schematic view of the CSM system, respectively. A pinhole with a 5  $\mu$ m diameter is exposed with the collimated EUV beam and the beam diameter is then reduced to improve the spatial coherence. A concave spherical

mirror and a plane turning mirror are then used to reflect the beam onto the EUV mask, and thus the pinhole image is relayed to the mask. The radius of curvature of the concave mirror is 200 mm, and the distance from the pinhole to the concave mirror is 200 mm, which is the same as the distance from the concave mirror to the mask. The mirrors are coated with 40 pairs of Mo/Si multilayers. Diffraction from the mask is recorded using a back-illuminated CCD camera. The CCD surface is placed parallel to the mask surface. The imaging area is 27.6×27.6 mm<sup>2</sup>, and contains 2048×2048 arrays of imaging pixels with an area of 13.5×13.5  $\mu$ m<sup>2</sup>. The angle of incidence from normal is 6° on the EUV mask, which matches the angle used in current EUV lithography scanners. The distance from the mask to the CCD camera is approximately 100 mm, which is equivalent to a numerical aperture (NA) of 0.14. The estimated spatial resolution is 59 nm.

A phase defect scatters EUV light illumination, where the signal depends on the phase distribution. When using conventional imaging optics, this phase distribution is recorded as a small dark spot on the detector caused by destructive interference. High magnification is required to characterize the defect. In contrast, the CSM can record the scattering signal directly, including the complex amplitude information of the defect. We have successfully reconstructed edge structure of line-and-space pattern from these scattering signals using a coherent diffraction imaging method.<sup>21-27)</sup> We have also succeeded in reconstructing both an intensity image and a phase image.<sup>19)</sup>

The sample mask was a blank EUV mask, which contained programmed bump structures on a glass substrate. The bumps were located with a 10  $\mu$ m pitch. The bump height was 7 nm, and the bump width was varied, ranging from 70 to 420 nm, with a square shape.



Fig. 1 Photograph of the CSM system. The arrows show the light path of the synchrotron radiation. The CCD camera records diffraction from the EUV mask pattern.



Fig. 2 Schematic view of the CSM system.

## Results

Figure 3 shows a diffraction image with a phase defect recorded using the CSM. The exposure time was 1,000 s. The intensity is shown in log scale. The defect was 420 nm wide and 7 nm high, as measured by atomic force microscopy (AFM). This defect had a truncated-pyramid shape with slope width of about 70 nm. The strong diffraction signal around the defect center was from the illumination. The Fraunhofer diffraction from the 5-µm-diameter entrance pinhole was recorded at the center position, as shown in Fig. 3. The illumination profile was asymmetric, because the small turning mirror limited the illumination pupil size. The center illumination signal was saturated because of the long exposure time, and the intensity was estimated to be  $8.8 \times 10^5$  counts from other data with shorter exposure times. Because the cross-shaped diffraction signal around the illumination came from the defect, the defect shape was determined to be a square. The diffraction signal intensity was about 30 counts, which was  $10^{-4}$  times weaker than the intensity at the illumination center. The defect width was estimated to be about 430 nm from the diffraction width of the crossed line, which corresponded well with the AFM value. The defect height was estimated to be 6.5 or 7.0 nm from the diffraction intensity ratio of the center to the crossed parts. The reflection phase change of the height was equal to 13.0 or 14.0 nm, which was a difference of 0.5 nm (0.23 rad) from the 13.5 nm EUV wavelength. Thus, the estimated height also corresponded well with the AFM value. We therefore successfully evaluated the defect width and height precisely using the CSM system.

Figure 4 shows diffraction images of defects with widths of (a) 420, (b) 220, and (c) 130 nm, and image (d) without a defect. The intensity was shown on a linear scale. All the defect heights were about 7 nm. The defect of 220 nm width also had a truncated-pyramid shape. Thus, the slope widths of (a) and (b) were about 70 nm at both sides, which was measured by AFM. That of the 130 nm-wide defect had a Gaussian shape. At the defect width of 420 nm shown in Fig. 4(a), the diffraction shape was easily recognized as a cross. However, because the diffraction spread to all

areas of the image of the 220 nm defect shown in Fig. 4(b), the defect shape could not be recognized with certainty. For the 130 nm defect, the diffraction intensity was almost the same as that of the sample without the defect. This signal was found to be speckle diffraction from the substrate roughness, which overlapped and hid the defect signal in the background. Figure 5 shows the diffraction signal profile of the indicated area shown in Fig. 4(a) as a white square. The center signal of the diffraction profile included the speckle noise signal of the fringed shape. The outside impulse signals were caused by the CCD camera noise. The profile of the 130 nm defect (dark-gray solid line) was similar to that of the image with no defect (dotted line), because the signal from such a small defect was hidden by the speckle noise.

The speckle noise was observed in the blank area with this mask. However, speckle noise was not observed in the other mask shown in Fig. 6. The exposed region was also a blank region without defects, where no speckle noise was recorded. The speckle signal was thus strongly dependent on the surface roughness, and would therefore degrade the detection limit size and precision of the defect characterization of the CSM system. George et al. reported that this speckle noise affects the line edge roughness.<sup>28)</sup> As a result, the surface should be smooth not only for multilayer reflectivity, but also for the aerial image quality. From the point of view of roughness evaluation, the CSM system was able to evaluate the actinic surface roughness of mask blanks precisely because it recorded the substrate speckle clearly. In comparison with another method using a photodiode detector<sup>29,30)</sup>, the CSM can record the two-dimensional speckle profile with a better S/N ratio, and evaluate the effect of speckle on the aerial image.



Fig. 3. Diffraction image with a programmed phase defect with 420 nm width and 7 nm height. The intensity is shown in log scale.



Fig. 4. Diffraction images of programmed phase defects of (a) 420, (b) 220, and (c) 130 nm width, and (d) an image without a defect. The intensity is shown on a linear scale.



Fig. 5. Intensity profile of the diffraction signals for the defects. The horizontal axis indicates the image position shown in Fig. 4(a).



Fig. 6. Diffraction image of a mask blank without defects. There is no speckle noise signal.

#### Discussion

- 4.1 Concept of micro-CSM system
  - The CSM system can evaluate defect properties
without any influence from the imaging optics. The CSM measured the defect width and height from the diffraction signals. However, small defect signals were hidden by the speckle noise because the defect signal was weak relative to the strong speckle noise from the surface roughness. Also, the illumination signal was 10<sup>4</sup> times stronger than the defect signal, making bright-field observation difficult. To minimize the noise and maximize the defect signal intensity, the illumination size should be as small as the defect size, which improves the defect-to-illumination size ratio. Thus, we propose the micro-CSM system shown in Fig. 7. The micro-CSM system has almost the same optics as the CSM system. The specific additional component in the micro-CSM is a Fresnel zone plate (FZP) that focuses the illumination onto a small phase defect. The FZP has an off-axis zone aperture, as shown in Fig. 7. Also, the diffraction from the defect transmits a rectangular aperture to the FZP membrane, which is recorded with a CCD camera directly. The target defect size of the micro-CSM system is 20 nm in width and 1 nm in height.



Fig. 7. Schematic view of micro-CSM system. Monochromatized EUV light is focused onto a defect by an off-axis Fresnel zone plate.

#### 4.2 Simulation of diffraction intensity profile

We simulated the diffraction signal from the defect with various illumination sizes to optimize the micro-CSM system. This simulation was based on scalar diffraction theory. The simulation conditions are as follows. The working wavelength was 13.5 nm. The illumination was focused using optics with an NA of 0.17. The angle of incidence was normal. The reflection from the multilayers on the substrate was assumed to be a reflection from a single layer for simplicity. The phase defect had a symmetrical circular shape, and a top-hat phase distribution. For speckle noise calculations, the reflection layer had a surface roughness of 0.15 nm (rms).

Figure 8 shows diffraction images from a phase defect with a diameter of 50 nm and a height of 1 nm. The illumination sizes were varied, with

diameters of (a) 1 µm and (b) 100 nm. The intensity is shown in log scale. The maximum NA position of the image was 0.5. The strong signal at the center originated from the illumination. The weak signal of the outside ring was a diffraction signal that came from the defect. For the 1-µm-diameter case, the speckle noise overlaps the defect signal. For the 100 nm case, there was no speckle noise, and the defect signal was recorded clearly. The intensity profiles of these images are shown in Fig. 9. The horizontal axis indicates the NA position at the detector, and the vertical axis indicates the signal intensity. The NA position corresponds to the diffraction angle. The intensities of the 1-µm- and 100-nm-diameter cases were normalized for the same illumination intensity. In the 1 µm case, the illumination peak signal was two orders stronger than that in the 100 nm case, while the defect signal was two orders weaker. The signal range spanned seven orders of magnitude, from  $10^{-5}$  to  $10^{2}$ . Because a typical CCD camera has a dynamic range of 4 orders of magnitude, it is difficult to record the defect signal using a CCD camera. Also, the speckle signal overlapped the defect signal, which was the same as that shown in Fig. 5. In the 100-nm-diameter case, the illumination and diffraction signal were recordable within three orders of magnitude, and no speckle signal was recorded. We thus chose the illumination size of 100 nm for the micro-CSM system, allowing the characterization of the defect using the CCD image.

We also simulated the diffraction signal profile from various sizes of defects with the 100-nm-diameter illumination. Figure 10(a) shows the diffraction signals from a defect with various heights ranging from 0 to 3 nm, while the width was fixed at a diameter of 50 nm. Figure 10(b) shows the diffraction for various diameters, ranging from 0 to 60 nm, while the height was fixed at 1 nm. The horizontal axis indicates NA positions at the detector same as Fig. 9. The illumination was assumed to have a top-hat intensity distribution for simplicity. Because the illumination size and the defect size were comparable for these conditions, the center signal decreases over 10% by destructive interference with the shallow 1-nm-height defect. Under these conditions, the defect position was detectable from the intensity change of the illumination signal. This was very useful for location of the defect position. Because the ABI tool has a low spatial resolution of 500 nm, scanning of the illumination using the micro-CSM system is necessary to characterize defects that are detected by the ABI tool. The diffraction profile for a tiny defect with a width of 20 nm was clearly different to the no-defect case. Thus, the detection limit of a defect signal using the micro-CSM is better than a defect with 20 nm width and 1 nm height, if the mask has

a low surface roughness of 0.15 nm (rms) and the sensor noise is negligible. Because the diffraction signals are very sensitive to the defect height and width, the micro-CSM can characterize the defect properties precisely.



Fig. 8. Calculated diffraction images with illumination diameters of (a) 1  $\mu$ m and (b) 100 nm. The defect has 50 nm diameter and 1 nm height. The substrate has 0.14 nm (rms) surface roughness.



Fig. 9. Intensity profiles of the calculated diffraction images shown in Fig. 8.





Fig. 10. Diffraction intensity profile with defects with various (a) widths and (b) heights.

#### Conclusions

Programmed phase defects on EUV mask blanks were observed using the CSM system. The CSM successfully detected phase defects down to a width of 220 nm, and we evaluated the defect width and height precisely for the 420 nm defect. This defect property information is important for repair using defect hiding and compensation methods with absorber pattern modulation. However, because the illumination diameter was as large as 5 µm, the defect signal was too weak. Also, the speckle noise signals from the substrates hid the defect signals for defect sizes smaller than 200 nm. We therefore proposed the micro-CSM system, which focuses the illumination onto the defect with a 100 nm diameter. Simulation results show that the micro-CSM system can record the diffraction signal clearly from a defect with a diameter of 20 nm and a height of 1 nm. As a result, the micro-CSM can characterize the defect properties. In a future work, we will construct the micro-CSM, and collect diffraction images from various programmed defects and actinic defects. The database relations between the ABI signals and the micro-CSM signals will help to enhance the ABI performance. The diffraction images recorded using the micro-CSM provides raw defect data, which is essential for defect compensation.

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# Chemical Reaction Analysis of EUV CA Resist using SR Absorption Spectroscopy

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It had been reported that tri-phenysulfonium cyclo(1,3-perfluoropropanedisulfone) imidate (TPS-IMIDATE) as a photo acid generator has approximately four times faster sensitive rather than tri-phenysulfonium perfluorobutanesulfonate (TPS-PFBS) under the EUV exposure. In this paper, we discussed the differences of the sensitivity and the chemical reaction between TPS-IMIDATE and TPS-PFBS, on the basis of the EUV-induced analysis of the SR absorption spectroscopy. From the analysis of the SR absorption spectroscopy, F and C atoms in the anion of TPS-IMIDATE decomposed rather than that of TPS-PFBS. The sensitivity advantage of TPS-IMIDATE might own to the anion decomposition reaction. The anion decomposition reaction might be originated to the photo-excitation of the photoacid generator. The anion of TPS-IMIDATE decomposed to smaller molecule and the sensitivity becomes higher.

Keyword: EUVL, chemically amplified resist, photoacid generator, decomposition of anion of PAG, SR absorption spectroscopy

#### 1. Introduction

Extreme ultraviolet lithography (EUVL) [1] is a promising lithographic technology which should begin to transfer to the production line for semiconductor electronics from the 25-nm node around 2013. The first top issue of EUVL is to achieve the EUV source power of 180 W at the intermediate focus position, when the resist sensitivity is assumed to be  $10 \text{ mJ/cm}^2$ . If the much higher sensitive resist can be performed, the EUV source power could be relaxed. In addition, the third issue of EUVL is to develop the EUV resist which has the sensitivity of  $10 \text{ mJ/cm}^2$  and the line width roughness (LWR) of smaller than 2 nm  $(3\sigma)$ because of the trade of relationship between the resolution, the LWR, and the sensitivity, so called "RLS" trade off. The photon number which the patterning requires for in EUV is approximately one order smaller than those in KrF

and ArF lithography. Thus, in order to achieve low LWR, the yield of the acid should increase. In addition, to achieve the high sensitivity and the low LWR, the acid production yield from the photoacid generators in the chemically amplifies resist [2-4] should increases.

In focusing, the production acid yield, the chemical reaction analysis on the basis of EUV photo irradiation should be performed in the basic study.[5-9]

In the previous report, for resist A, the peak at the absorbance at 1156 cm<sup>-1</sup> in the fourier transform infrared (FT-IR) spectra increased after EUV exposure.[7-9] However, there was no change in the FT-IR spectra of resist B before and after EUV exposure. As a results of the electron orbital calculation using perturbation theory by the software code Gaussion03 [10], the peak at approximately 1156 cm<sup>-1</sup> in FT-IR spetra of resist A corresponds to C-F bonding of the anion of

As a result, the outgassing TPS-IMIDATE. measurements and the FT-IR spectra measurements indicated that the EUV-induced reaction of **TPS-IMIDATE** occurred more efficiently than that of TPS-PFBS. To clarify the difference of the anion decomposition, the analysis using SR spectroscopy is performed. This paper focused on the chemical reaction analysis of the model chemically amplified resists by the SR absorption spectroscopy.

#### 2.Experimental

#### 2.1. Materials

The model resists which were employed in this study are shown in Table 1. The resists A and B is employed poly (hydroxystyreneco-t-butylacrylate) as the base polymer, and monomethyletheracetate propyleneglycol (PGMEA) as a solvent. Resists A and B employed triphenylsulfonium cyclo(1,3- perfluoro propanedisulfone) imidate (TPS-IMIDATE) and triphenylsulfonium perfluorobutanesulfonate (TPS-PFBS) as the photoacid generator, respectively. The PAG content is approximately 30 wt% of the base polymer to increase the detection S/N ratio of the anion decomposition species from the PAG in the SR spectroscopy measurement before and after EUV exposure. The resist solution was spin coated on a 4-inches silicon wafer to be a 50-nm-thickness. The film thickness was Nanometrics measured by 6100A (NANOmetrics). The prebake conditions was carried out on a hot plate at the temperature of 130°C in the time period of 90 s.





#### 2.3. SR Absorption Experiment

The SR absorption spectroscopy measurements were performed at the end station of the BL07B beamline at the NewSUBARU synchrotron radiation facility. The short undulator was employed as a light source of this beamline. The configuration setup of the BL07B is shown in Fig.1. The beamline consists of three glancing mirros such as M0, M1 and M2, the monochromater (G), the entrance (S1) and exit (S2) slits and the end station exposure and analyzing chambers. The loadlock chamber was adapted to these chambers to exchange the sample. The photography of the BL07B beamline and the end station are shown in Figs.2(a) and 2(b). The variable line spacing plane gratings (VLSPG) were employed as monochromator. Three density types such as 600, 1200, and 2400 lines/mm were installed in the monochromator vacuum chamber. The photon energy region is from 80 eV and 800 eV in the



Fig. 1 System configuration of the BL07B beamline.

SR spectroscopy. The exit slit size is 20  $\mu$ m(H)×20  $\mu$ m(V) and the SR light spot size on a sample is 1 mm(H)×1 mm (V). The energy resolution  $E/\Delta E$  is approximately 1000. The photon flux of the photon energy of 91.8 eV ( $\lambda$ =13.5 nm) is approximately 3.0×10<sup>11</sup> photons/s/100mA.

The absorption signal was obtained from the ratio of the photocurrent from the sample to the photocurrent from the gold mesh. The total energy resolution was  $\sim 0.5$  eV. The photocurrent was measured by the electrometer (6514, Keithley).

For the absorption measurement of F 1s core level, the measured energy region is 685-735 eV and 2400 lines/mm VLSPG was employed with the undulator gap of 52.0 mm. For the absorption measurement of C 1s core level, the measured energy region is 280-330 eV and 1200 lines/mm VLSPG was employed with the undulator gap of 48.0 mm. For the absorption measurement of N 1s core level, the measured energy region is  $390 \sim 440 \text{ eV}$  and 2400 lines/mm VLSG was employed with the undulator gap of 51.0 mm. The electron current generated on the sample is measured in the SR absorption experiment during the SR light exposure.





Fig. 2 Photographs of (a) BL07B beamline and (b) end station.

#### 3. Results and Discussions

#### 3.1. SR Absorption Spectra

SR absorption spectra of F 1s core level at the photon-energy ranges of 685-735 eV of resists A and B are shown in Figs. 3 (a) and 3(b), respectively. For resist A, the absorption at the photon energy of 697 eV decreased when the EUV exposure dose increased and the absorption disappeared at the EUV dose of  $104 \text{ mJ/cm}^2$ . For resist B, the absorption at the photon energy of 697 eV decreased when the EUV exposure dose increased. However, the absorption signal remained at the EUV exposure dose of  $104 \text{ mJ/cm}^2$ . The EUV exposure dose dependency of the absorption of F atoms at the photon energy of 697 eV is shown in Fig. 4. The decomposition of F atoms in the anion of the TPS-IMIDATE has easier to decompose than that of TPS- PFBS.

As the results, F atoms decomposition speed of the TPS-IMIDATE is faster than that of the TP- PFBS.



Fig. 3 Absorption spectra of F 1s core level in the anions of (a) TPS-IMIDATE and (b) TPS- PFBS.



Fig. 4 EUV exposure dose dependency of the absorption of F 1s core level at the photon energy of 697 eV.

Absorption spectra of C 1s core level at the photon-energy ranges of 280-330 eV of resists A and B are shown in Figs. 5 (a) and 5(b), respectively.

For resist A, the absorption at the photon energy of 287 eV had no change. Thus, it means that the  $\pi$ -bonding of the benzyl group of the base polymer has no change. However, the absorption at the photon energy of 290 eV decreased after the EUV exposure. It means that the anion of the  $\sigma$ -bonding of the anion of TPS-IMIDATE decomposed under the EUV exposure.

For resist B, the absorption at the photon energy of 290 eV had no change before and after the EUV exposure. It means that the anion of the  $\sigma$ -bonding of the anion of TPS-IMIDATE decomposed under the EUV exposure.

Absorption spectra of N 1s core level at the photon-energy ranges of 390-440 eV of resist A is shown in Fig.6. the absorption at the photon energy of 405 eV decreased under the EUV exposure. And the photo-energy of 403 eV increased under EUV exposure and the chemical shift was observed. It means that N atoms in the anion of TPS-IMIDATE decomposed and reconstructed under the EUV exposure.

As the results of the SR spectroscopy, the  $\sigma$ -bonding of the anion of TPS-IMIDATE decomposed to the small molecule size and the acid diffusion length might become large. Thus the sensitivity of resist A might become

much higher than that of resist B.



Fig. 5 Absorption spectra of C 1s core level of the anions of (a) TPS-IMIDATE and (b) TPS- PFBS.



Fig. 6 Absorption spectra of N 1s core level in the TPS-IMIDATE anion.

#### 4. Conclusion

As the analysis results of the SR spectroscopy measurement, it was confirmed that the decomposition reaction begin to occur by the absorption by the EUV photons at F

atoms in the anion of TPS-IMIADTE and the anion molecular size becomes smaller than the original one. However, for resist B, only F atoms in the anion of TPS-PFBS decomposed and the molecular size of the anion did not dramatically change. Since the anion size of TPS-IMIDATE might be much smaller than that of TPS-PFBS, the acid diffusion length in resist A might become larger than that in resist B.

To achieve the low LWR, it had introduced generally that the diffusion length of PAG should decreased by increasing the molecular size of the anion of PAG. However, for the anion PAG which include F atoms, from the results of the SR spectroscopy, F atoms might decompose under EUV exposure. Therefore, since the anion of the PAG which includes F atoms should be analyzed carefully if the decomposition reaction of the anion of PAG would occur or not.

The SR absorption spectroscopy might be a powerful analysis method to analyze the decomposition reaction of the anion of PAG. To satisfy the specification of the EUV resist which require for high volume manufacturing, all the chemical reaction should be taken in account.

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### **Plasma-Debris Sputter Resistant X-ray Mirror**

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#### Abstract

A diamond-like carbon (DLC) mirror, used as a grazing incident mirror in a plasma X-ray source, exhibits a high resistance to plasma debris sputtering. The erosion rate due to plasma debris sputtered at the incident debris angle of 20° was measured using a laser-produced Xe plasma source developed by the authors. The results indicate that the DLC film has a 5- and 15-fold higher sputtering resistance compared to films made of the traditional mirror materials Ru and Au, respectively. Because the DLC mirror retains a high sputtering resistance to Sn ions, it may be effective in Sn plasma source applications. We conclude that a grazing incident X-ray mirror coated with DLC can be of use as a plasma debris sputtering resistant mirror.

Plasma X-ray sources, which produce radiation from laser-produced plasmas (LPP) or dischargeproduced plasmas (DPP), find use in various industrial applications. However, along with Xrays, the plasmas in these sources emit debris consisting of ions, neutral atoms, various fragments, vapor and so forth. Such debris damages mirrors located near the plasma, quickly degrading their reflectivity. Because the amount of plasma debris increases in proportion to the Xray generating power, the debris problem is a critical issue in high-power plasma sources for industrial applications. We propose a new approach to mitigate debris effects in plasma Xray sources, namely the use of debris resistant mirrors that suffer reduced debris damage as compared with traditional mirrors.

In our lab, we developed a laser-produced plasma X-ray source (LPX), which employs a solid Xe target. This device has demonstrated continuous X-ray generation at 5–17 nm with an average power of 20 W. A diamond-like carbon (DLC) coating, also developed in our laboratory, was deemed a good candidate for the mirror material, owing to its high hardness. In this work, we measured the erosion rate due to debris sputtering in the plasma source. The results were compared with similar experiments with mirrors coated with Ru and Au films, which are typically used as mirror coating materials.

The LPX consists of a system that supplies a solid Xe-target and a drive laser. The target supply system comprises a cylindrical drum filled with liquid nitrogen, so its copper surface is at liquid nitrogen temperature. Xe gas blown onto this surface condenses to form a solid Xe layer. The solid Xe layer-coated drum rotates about the vertical axis, simultaneously moving up and down vertically during rotation. The resultant spiral motion ensures that a fresh target surface is continuously supplied for every laser shot. The drive laser is a slab laser with an average power of 100 W and a pulse repetition rate of 320 Hz. The laser pulses ( $\lambda = 1064$  nm) with a pulse width

of 20 ns are focused on the solid Xe-target, continuously producing plasma.

We used a quartz crystal microbalance (QCM) to measure the erosion rate of the DLC films after sputtering with Xe plasma debris from the LPX. As such debris bombards a test film that is coated onto the QCM, atoms are ejected from the surface of the film, changing the resonant frequency of the QCM. Mass loss in the film can be deduced from this frequency change, and erosion rates of the film can be calculated directly. The experimental setup is shown in Fig.1.



Figure 1. Experimental setup.

The drum target system and the QCM were installed in a vacuum chamber (pressure of 0.2Pa), while drive laser pulses coming through a window were focused perpendicularly onto the target by a lens. The coated QCM was placed 73 mm from the plasma at a 45° angle with respect to the incident laser beam. Its sensor surface was tilted at a 20° angle with respect to the incident debris axis, thus forming a grazing incidence mirror. Test films coated on the quartz sensors consisted of DLC, Ru and Au, with a coating thickness of 500, 100, and 100 nm, respectively. After laser irradiation of the films for 2–10 min at 320 Hz, we used the QCM to monitor total erosion rates during extended multi-shot plasma operation.

The measured erosion rates of the DLC, Ru and Au films at an incident debris angle of 20° are shown in Fig. 2. We see a decreased erosion rate with increasing binding energy, and the erosion rate ratio is DLC : Ru : Au = 1 : 5 : 15. We also performed an erosion calculation using the SRIM software. SRIM can calculate a sputtering yield  $Y_{\text{sputt}}$  for normal carbon, Ru and Au. For a given sputtering yield  $Y_{\text{sputt}}$  (atoms / ion) and an ion flux  $F_{\text{ion}}$  (ions), the erosion rate of a mirror film  $\Delta T$  (cm / shot) can be written as:

$$\Delta T = Y_{sputt} \cdot F_{ion} \cdot \frac{m}{\rho}$$

where *m* is the mirror mass (g) and  $\rho$  is the mirror density (g/cm<sup>2</sup>).

The plasma debris emitted from the LPX was studied in detail previously, with the results indicating the debris predominantly consists of fast ions. The time of flight (TOF) Xe ion signal as detected by a Faraday-cup indicated the ion energy is less than 6 keV, and the ion flux at the QCM was calculated to be about  $6 \times 10^{11}$  /shot. Using this result as the ion flux  $F_{ion}$  and the calculated sputtering yield  $Y_{\text{sputt}}$  in the eq., we can predict the erosion rates  $\Delta T$  for the three films. The ratios of these calculated values are C : Ru : Au = 2 : 6 : 16, which are close to the experimental results of 1:5:15. Compared with the calculated erosion rate for C, the measured value for the DLC is slightly smaller. This difference may be due to the different types of carbon involved: high hardness DLC in the experiment vs. normal carbon (graphite) in the calculation.



Figure 2. Erosion rate of the DLC, Ru, and Au films as measured by QCM with a debris incidence angle of  $20^{\circ}$ .

Sn DPP X-ray sources are currently used as extreme ultraviolet lithography (EUVL) sources in the industrial mass production of semiconductors. These sources emit X-rays at a wavelength of 13.5nm, and employ grazing incidence Ru mirrors. As shown in Fig.3, the DLC sputtering yield by Sn ions is similar to the one by Xe ions, as calculated by the SRIM code. Therefore, a DLC mirror may also be resistant to Sn sputtering. Of course, because the Sn plasma debris includes both "deposition" and "sputter" types of particles, additional debris mitigation techniques are necessary. However, we predict that a DLC mirror will enjoy a longer lifetime in a Sn plasma source.



Figure 3. DLC sputtering yield by Xe and Sn ions, calculated with the SRIM code.

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## **Electronic Structure of the Fluorinated Self-Assemble Monolayer by Photoemission and Absorption Spectroscopy**

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#### Abstract

The electronic structure of F-SAMs (fluorinated self-assembled monolayer) thin films with different chain length was investigated by the photoelectron and absorption spectroscopy. The photoelectron spectra in the wide region and in the C 1s core-level region were measured and the chemical compositions and components of the photoelectron spectra F-SAMs thin films with different chain length were clarified. In addition, the C K-edge absorption spectra of F-SAMs thin films were measured and the several spectral features in absorption spectra of the F-SAMs thin films were assigned. Based on the results of the photoelectron and absorption spectroscopy measurements of four kinds of F-SAMs with different chain length, the electronic structure of the F-SAMs thin films is discussed.

#### Introduction

The study of nanoimprint lithography (NIL) [1-2] has attracted much attention for many industrial field because it is a promising method to fabricate various nanostructures with a low cost and a high throughput. In the process of NIL, the mold is usually coated with an antisticking layer to avoid resist adhesion. As an antisticking layer of nanoimprint mold, the fluorinated self-assemble monolayer (F-SAM) is used, for example. The evaluation of the F-SAM with different chain length is one of the critical issues in NIL [3]. In this study, four kinds of F-SAMs with different chain length were evaluated using the photoemission and the absorption spectroscopy.

#### Experiments

Four kinds of F-SAMs were prepared from a precursor  $[CF_3(CF_2)_n(CH_2)_2Si(OCH_3)_3; n=0, 3, 5,$ and 7] as denoted FAS-3, 9, 13, and 17, respectively. All photoelectron and absorption measurements were performed on a BL7B end station at the NewSUBARU facility, University of Hyogo. The photoelectron spectra were measured in an analysis chamber mounted with a hemispherical electrostatic spectrometer (VSW Ltd, CL150). The synchrotron radiation and the Mg K $\alpha$  line were used as the excitation source and were incident at 45° with respect to the surface normal. The total energy resolutions were about 0.7 eV for the C 1s core-level regions. Gold films evaporated on copper sample holders and F-SAMs were used for the Fermi level measurements and the total energy resolution reference. Absorption spectra were measured by the total electron yield method. The total energy resolution was about 0.5 eV. The photocurrents from the sample and from a gold mesh were recorded simultaneously. The absorption signal was obtained from the ratio of the photocurrent from the sample to the photocurrent from the gold mesh.

#### Results

Figure 2 shows the photoelectron spectra in four kinds of F-SAMs with different chain length. The photoelectron spectrum of Si substrate is also plotted for comparison. Several peaks were observed at ~688, ~532, ~290, ~100eV, which



Figure 1. Four kinds of F-SAM thin films with different chain length.



Figure 2. Wide scan of the photoelectron spectra of the four kinds of F-SAMs thin films with different chain length. The photoelectron spectra in this figure were normalized by the C 1s peak intensity.

were originated from the F 1s, O 1s, C 1s, and Si 2p electrons, respectively. With increasing the chain length, the intensity of the peak at ~688eV increased while intensity of the peaks at ~532 and ~100eV decreased. On the other hand, the intensity of the peaks at ~ 290 eV did not change with increasing the chain length. These indicate that the intensity of the Si substrate decreased due to the increase of thickness of F-SAM with increasing the chain length. In Figure 3, the photoelectron spectra of the C 1s core-level region in four kinds of F-SAMs with different chain length are plotted. In the photoelectron spectra of the C 1s core-level, three peaks at ~293, ~286, and ~284.5 eV were observed in the FAS-3 although four peaks at ~293, ~291, ~286, and ~284.5 eV were observed in the FAS-9, 13, and 17. The intensity of the peak at 291 eV increased with increasing the chain length. On the other hand, the intensity of the peaks at ~293, ~286 eV did not change with increasing the chain length. From the chemical compositions of four kinds of F-SAMs with different chain length, these peaks at ~293, ~291, ~286, and ~284.5 eV were assigned to the CF<sub>3</sub>, CF<sub>2</sub>, CH, and C-C components, respectively. Figure 4 shows the absorption spectra in four kinds of F-SAMs with different chain length. Several peaks were observed at 285, 292, 295, 296-300eV. The intensity of the peak at 292eV increased with increasing the chain length. On the other hand, the intensity of the peaks at 285, 295, 296-300eV did not change with increasing the chain length. The peaks at 292 eV were assigned to the  $\sigma^{*}(C-F)$  and  $\sigma(CF_{2})$  components. On the other hand, these peaks at 285, 295, and 296-300 eV were assigned to the  $\pi^*(C-C)$  and  $\sigma^*(C-H)$ ,  $\sigma^*(C-F)$  and  $\pi(CF_3)$ , and  $\sigma^*(C-F)$ ,  $\sigma(CF_2, CF_3)$ ,  $\sigma^*(C-C)$  components, respectively [4]. When the incident angle of the synchrotron radiation to the sample surface was changed, no clear change of the absorption spectra was not observed in four kinds of F-SAMs with different chain length. This indicates that each molecular with different chain length on the Si surface seems to be oriented randomly.



Figure 3. Photoelectron spectra of the C 1s core-level region in four kinds of F-SAMs thin films with different chain length.



Figure 4. C K-edge absorption spectra in four kinds of F-SAMs with different chain length.

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### Orientation evaluation of 3D-photoreactive liquid crystalline polymer structure fabricated by thermal nanoimprinting

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#### Abstract

Photoreactive liquid crystalline polymer is able to be control by linearly polarized ultra violet (LPUV) irradiation and heat treatment. We found that P6CAM, which is one of the photoreactive liquid crystalline polymers, was reoriented by thermal nanoimprinting. It is confirmed that the P6CAM molecules were reoriented parallel to the imprinted line. To examine whether the two molecular orientation directions are induced on the P6CAM film, we carried out thermal nanoimprinting using a mold with 3D structure pattern. As the results, the P6CAM 3D structure has two molecular orientation directions.

#### Introduction.

The photo-induced orientation of polymeric films has received much attention due to its potential use in many kinds of optical and photonics applications. P6CAM, which is a one of the photoreactive liquid crystalline polymers, exhibits a large photoinduced molecular reorientation with a high photoreactivity toward linearly polarized UV (LPUV) light and heat treatment [1, 2]. We found that P6CAM was aligned by thermal nanoimprinting[3] using line and space (L&S) pattern mold [4]. We confirmed that the P6CAM molecules were reoriented parallel to the imprinted line on the imprinted P6CAM film in the case of using a normal L&S pattern mold. If a mold with bidirectional L&S pattern is used for the thermal nanoimprint on the P6CAM, two reorientation directions of the molecules according to the bidirectional mold pattern may be induced. To confirm that, we fabricated the bidirectional line pattern mold by electron beam (EB) lithography and reactive ion etching (RIE) and then carried out thermal nanoimprinting using this mold on the P6CAM film on a glass substrate, subsequently evaluated the molecular orientation by measuring the diffraction efficiency.

# Fabrication of bidirectional line pattern on P6CAM

Figure 1 shows the illustration of bidirectional line pattern. The linewidth was 2  $\mu$ m. The line heights were 200 and 100 nm. The two line patterns crossed each other at right angles. The

mold was coated with an antisticking layer. We used a thin polydimethylsiloxane (PDMS) layer as the antisticking layer [5]. We carried out thermal nanoimprinting using this mold.



Fig. 1 Illustration of bidirectional line pattern.

The P6CAM was spin-coated on the glass substrate. The mold and P6CAM substrate were heated by 165 °C during thermal nanoimprinting. The imprinting pressure and pressing time were 15 MPa and 4 min, respectively. After thermal nanoimprinting, we observed the fabricated P6CAM structure by POM under crossed-nicols and atomic force microscopy (AFM), as shown in Fig. 2. The POM image showed the pattern contrast which means the molecular orientation related the pattern configuration. In addition, the 3D structure was successfully imprinted on P6CAM, as shown in Fig. 2(b).



Fig. 2 (a) POM and (b) AFM images of fabricated 3D-P6CAM structure.

# Evaluation of molecular orientation of imprinted P6CAM-3D-structure

We examined the orientation direction of the P6CAM 3D structure by measuring the diffraction efficiencies using linearly polarized (LP) 633-nm light from  $0^{\circ}$  to  $180^{\circ}$ . If the P6CAM is reoriented by thermal nanoimprinting, the diffraction efficiency depend on the rotation angle of the incident LP light.



Fig. 3 (a) Relationship between directions of incident LP light and imprinted lines in the optical measurement. (b) Diffraction efficiencies of P6CAM 3D structure.

Figure 3(a) shows the relationship between directions of incident LP light and imprinted lines in the optical measurement. When the rotation angle of incident LP light was 0°, the LP light direction is parallel to the 200 nm-height-line pattern. At 90°, the LP light direction is perpendicularly to the 200 nm-height-line. On the other hand, in the case of the 100 nm-height line pattern, the LP light directions at 0° and 90° are perpendicularly and parallel to the line pattern, respectively. When the P6CAM orientation and incident LP light directions are the same, the

1st-order diffraction efficiency is highest. Figure 3(b) plots the 0th and 1st-order diffraction efficiencies of the P6CAM 3D structure as a function of the incident polarization angle. The diffraction efficiency depend on the rotation angle of the incident LP light. In addition, the diffraction efficiency of the 1st-order diffracted light of the 200 nm-height-line pattern was the highest at 0° and the lowest at 90°. In contrast, that of the 100 nm-height line pattern was the lowest at 0° and the highest at 90°. These results indicates that the P6CAM was reoriented parallel to each line.

#### Conclusion

We carried out thermal nanoimprinting using the bidirectional line pattern mold and evaluated the orientation of the fabricated P6CAM 3D structure. The P6CAM 3D structure was successfully fabricated by thermal nanoimprinting. In addition, the P6CAM 3D structure has two molecular orientation directions and the reorientation direction was parallel to the line. This means that we are able to arbitrarily control the P6CAM molecular orientation by thermal nanoimprinting.

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# **List of Publications**

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- 2. Shuji Miyamoto, "Gamma-ray Beambeamline on NewSUBARU", "Science and Technology with MeV Photons at Canadian Light Source", Uiv. of Saskatuwan, Jan. 18-19 (2013).
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- Yuji Yoritama, T. Uchiyama, Akinobu Yamaguchi, Yuichi Utsumi, "Fabrication of Integrated Magneto Impedance Sensor for Medical Monitoring", 38th International Conference on Micro and Nano Engineering (MNE2012), p298-378, September 16-20 (2012), Toulouse, France
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- 63. S. Iyoshi, M. Okada, Y. Haruyama, S. Matsui, K. Kobayashi, S. Kaneko, M. Nakagawa, H. Hiroshima, "Study of demolding Characteristics in continuous UV nanoimprinting", The 56th International Conference on electron, ion, photon beam technology and fabrication, Hawaii, 2012/5/30
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- M. Chinen, Y. Kang, M. Okada, Y. Haruyama, H. Hiroshima and S. Matsui, "Evaluation of Interaction Force between UV Resin and F-SAMs by Dynamic Contact Angle Measurement in PFP Gas Ambient", 25th International Microprocesses and Nanotechnology Conference, Kobe, 2012/11/2

# **Academic Degrees**

# Academic Degree

Degree	Name	Master's Thesis
Master of Science	<b>Daisuke Tonaka</b> (University of Hyogo)	Development and evaluation of energy band expansion of laser Compton scattering gamma-ray source
Master of Science	<b>Yousuke Hamada</b> (University of Hyogo)	Stabilization of electron storage ring by auto adjustment of betatron tune
Master of Science	Yasuhisa KITAGAWA (University of Hyogo)	Study on Evaluation of Laser Compton Scattering Gamma-ray Source
Master of Science	<b>Sayaka CHIN</b> (University of Hyogo)	Development of THz radiation Source by Compact LINAC LEENA
Master Of Engineering	<b>Takuya KOTAKA</b> (University of Hyogo)	Development of spectroscopic methods using soft X-ray emissions in BL9a at the NewSUBARU SR facility
Master of Engineering	<b>Luo WULIN</b> (University of Hyogo)	Fabrication of flexible light guide plate using hot-embossment
Master of Engineering	<b>Zhu XIAOZI</b> (University of Hyogo)	Hot-embossing fabrication of diffraction grating with narrow line width
Master of Engineering	Yuu KUBOYAMA (University of Hyogo)	Evaluation of compact capacitance type inclination sensor fabricated by LIGA process
Master of Engineering	Yuji YORITAMA (University of Hyogo)	Study on microfabrication process for magnetic and optical devices
Master of Engineering	Hiroki NOSE (University of Hyogo)	Study on full protocol control using three-dimensional Lab-on-a-CD
Master of Engineering	Masato NAKASUJI (University of Hyogo)	Development of the coherent EUV scatterometry microscope with the high-order-harmonic generation EUV source
Master of Engineering	<b>Takuro URAYAMA</b> (University of Hyogo)	Development of the EUV interference lithography system for the evaluation of 1x-nm-node EUV resist
Master of Engineering	Akifumi TOKIMASA (University of Hyogo)	Development of the EUV microscope using a high-magnification objective for the EUV mask evaluation
Master of Science	Mika CHINEN (University of Hyogo)	Study of release property of UV resin and antisticking layer in PFP gas ambient by contact angle measurement
Master of Science	Yohei SAWADA (University of Hyogo)	Study of curing process of UV nanoimprint resin

Degree	Name	Docter's Thesis
Docter of	Tomoaki INOUE	Study on intense soft X-ray generator using laser-produced plasma
Engineering	(University of Hyogo)	

# Cover photographs

## 15MeV Compact Electron Linear Accelerator LEENA

Using relativistic electron beams of a compact electron linear accelerator LEENA, the development of terahertz radiation sources is in progress at our laboratory.

Electron beams from a RF gun with a thermal cathode are bunched at an alpha magnet and accelerated by a 15 MeV standing wave linac.

Smith-Purcell light in terahertz regime is emitted from a surface of metal, when an electron passes through the neighborhood of the metal grating.

The light was taken out from a vacuum chamber by three movable mirrors into the atmosphere.

The wavenumber spectrum of the light is measured with Martin-Puplett interferometer, in which wire grid polarizer is used to split terahertz light.



"Smith-Purcell grating and mirrors in the vacuum chamber."

"Martin-Puplett interferometer."
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